



## ELECTRICAL-AND-THERMOELECTRIC PROPERTIES, OBTAINED IN N(P)-TYPE DEGENERATE $\text{InSb}_{1-x}\text{As}_x$ -CRYSTALLINE ALLOY

(I)

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**ABSTRACT**

In the  $n^+(p^+) - p(n)$   $\text{InSb}_{1-x}\text{As}_x$ -crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018; Van Cong et al., 1984), are now revised and performed, by basing on our basic expressions, given Equations (1, 3, 5, 7, 11, 14, 19). Some remarkable results could be cited in the following. In Tables 5n (5p) given Appendix 1, for a given impurity density  $N$  and with increasing temperature  $T$ , and then in Tables 6n(6p) given Appendix 1, for a given  $T$  and with decreasing  $N$ , the reduced Fermi-energy  $\xi_{n(p)}$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). Further, one notes in these Tables that with increasing  $T$  (or with decreasing  $N$ ) one obtains: (i) for  $\xi_{n(p)} \simeq 1.8138$ , while the numerical results of the Seebeck coefficient  $S$  present a **same**

**minimum**  $(S)_{\min.} (\simeq -1.563 \times 10^{-4} \frac{V}{K})$ , those of the figure of merit  $ZT$  show a **same maximum**  $(ZT)_{\max.} = 1$ , (ii) for  $\xi_{n(p)} = 1$ ,  $S$ ,  $ZT$ , the Mott figure of merit  $(ZT)_{\text{Mott}}$ , the Van-Cong coefficient  $VC$ , and the Thomson coefficient  $Ts$  present **the same results**:  $-1.322 \times 10^{-4} \frac{V}{K}$ , 0.715, 3.290,  $-1.105 \times 10^{-4} \frac{V}{K}$ , and  $1.657 \times 10^{-4} \frac{V}{K}$ , respectively, and (iii) for  $\xi_n \simeq 1.8138$ ,  $(ZT)_{\text{Mott}} = 1$ . It seems that these same results could present a new law in the thermoelectric properties, obtained in the degenerate case.

**KEYWORDS:** Electrical conductivity, Seebeck coefficient, Figure of merit, Van-Cong coefficient, Thomson coefficient, Peltier coefficient.

## INTRODUCTION

In the  $n^+(p^+) - p(n)$   $\text{InSb}_{1-x}\text{As}_x$ - crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018; Van Cong et al., 1984), are now revised and performed, by basing on our following basic expressions (Van Cong, 1980 and 2024; Van Cong and Debiais, 1993; Van Cong and Doan Khanh, 1992).

(1) The effective extrinsic static dielectric constant law,  $\varepsilon(r_{d(a)}, x)$ , due to the impurity size effect, is determined in Eq. (1).

(2) The generalized Mott criterium in the metal-insulator transition is expressed in Equations (3, 5, 6), showing that  $N_{\text{CDn(CDp)}}$  is just **the density of electrons (holes) localized in the exponential conduction (valence)-band tail**,  $N_{\text{CDn(CDp)}}^{\text{EBT}}$ , with a precision of the order of  $2.86 \times 10^{-7}$ , as given in our recent work (Van Cong, 2024), and the effective electron (hole)-density:  $N^* \equiv N - N_{\text{CDn(CDp)}} \simeq N - N_{\text{CDn(CDp)}}^{\text{EBT}}$ , as that observed in the compensated crystals.

(3) The ratio of the inverse effective screening length  $k_{\text{sn(sp)}}$  to Fermi wave number  $k_{\text{Fn(kp)}}$  at 0 K,  $R_{\text{sn(sp)}}(N^*)$ , defined in Eq. (7), is valid at any density  $N^*$ .

(4) The Fermi energy for any N and T,  $E_{\text{Fn(Fp)}}$ , determined in Eq. (11) with a precision of the order of  $2.11 \times 10^{-4}$  (Van Cong, 1993), and it is present in all the expressions of electrical-and-thermoelectric coefficients.

(v) Our expressions for the electrical conductivity,  $\sigma$ , and for the Seebeck coefficient, S, determined respectively in Equations (14, 19) are the basic expressions for determining the following electrical-and-thermoelectric coefficients.

## OUR STATIC DIELECTRIC CONSTANT LAW-AND-GENERALIZED MOTT CRITERIUM IN THE METAL-INSULATOR TRANSITION

First of all, in the  $n^+(p^+) - p(n)$   $\text{X(x)} \equiv \text{InSb}_{1-x}\text{As}_x$ - crystalline alloy at  $T=0$  K, we denote the donor (acceptor) d(a)-radius by  $r_{d(a)}$ , the corresponding intrinsic one by:  $r_{\text{do(ao)}} = r_{\text{Sb(In)}}$ ,

the unperturbed relative effective electron (hole) mass in conduction (valence) bands by:  $m_{c(v)}(\mathbf{x})/m_o$ , the unperturbed relative static dielectric constant by:  $\epsilon_o(\mathbf{x})$ . Then, their values are reported in **Table 1 in Appendix 1**.

Therefore, we can define the effective donor (acceptor)-ionization energy in absolute values as:

$$E_{do(ao)}(\mathbf{x}) = \frac{13600 \times [m_{c(v)}(\mathbf{x})/m_o]}{[\epsilon_o(\mathbf{x})]^2} \text{ meV} , \text{ and then, the isothermal bulk modulus, by:}$$

$$B_{do(ao)}(\mathbf{x}) \equiv \frac{E_{do(ao)}(\mathbf{x})}{\left(\frac{4\pi}{3}\right) \times (r_{do(ao)})^3} .$$

**Effect of Impurity  $r_{d(a)}$ -size, with a given  $\mathbf{x}$**

Here, the changes in all the energy-band-structure parameters, expressed in terms of the effective relative dielectric constant  $\epsilon(r_{d(a)}, \mathbf{x})$ , developed as follows.

At  $r_{d(a)} = r_{do(ao)}$ , the needed boundary conditions are found to be, for the impurity-atom volume  $V = (4\pi/3) \times (r_{d(a)})^3$ ,  $V_{do(ao)} = (4\pi/3) \times (r_{do(ao)})^3$ , for the pressure  $p$ ,  $p_o = 0$ , and for the deformation potential energy (or the strain energy)  $\sigma$ ,  $\sigma_o = 0$ . Further, the two important equations (Van Cong, 1984 and 2018), used to determine the  $\sigma$ -variation,  $\Delta\sigma \equiv \sigma - \sigma_o = \sigma$ , are defined by:  $\frac{dp}{dV} = -\frac{B}{V}$  and  $p = -\frac{d\sigma}{dV}$ . giving:  $\frac{d}{dV}\left(\frac{d\sigma}{dV}\right) = \frac{B}{V}$ . Then, by an integration, one gets:

$$\left[\Delta\sigma(r_{d(a)}, \mathbf{x})\right]_{n(p)} = B_{do(ao)}(\mathbf{x}) \times (V - V_{do(ao)}) \times \ln\left(\frac{V}{V_{do(ao)}}\right) = E_{do(ao)}(\mathbf{x}) \times \left[\left(\frac{r_{d(a)}}{r_{do(ao)}}\right)^3 - 1\right] \times \ln\left(\frac{r_{d(a)}}{r_{do(ao)}}\right)^3 \geq 0.$$

Furthermore, we also shown that, as  $r_{d(a)} > r_{do(ao)}$  ( $r_{d(a)} < r_{do(ao)}$ ), the compression (dilatation) gives rise to the increase (the decrease) in the energy gap  $E_{gn(gp)}(r_{d(a)}, \mathbf{x})$ , and the effective donor (acceptor)-ionization energy  $E_{d(a)}(r_{d(a)}, \mathbf{x})$  in absolute values, obtained in the effective Bohr model, which is represented respectively by:  $\pm [\Delta\sigma(r_{d(a)}, \mathbf{x})]_{n(p)}$ ,

$$E_{gno(gp_o)}(r_{d(a)}, \mathbf{x}) - E_{go}(\mathbf{x}) = E_{d(a)}(r_{d(a)}, \mathbf{x}) - E_{do(ao)}(\mathbf{x}) = E_{do(ao)}(\mathbf{x}) \times \left[ \left(\frac{\epsilon_o(\mathbf{x})}{\epsilon(r_{d(a)})}\right)^2 - 1 \right] + [\Delta\sigma(r_{d(a)}, \mathbf{x})]_{n(p)} ,$$

for  $r_{d(a)} \geq r_{do(ao)}$ , and for  $r_{d(a)} \leq r_{do(ao)}$ ,

$$E_{\text{gno}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d}(\text{a})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{do}(\text{ao})}(\mathbf{x}) = E_{\text{do}(\text{ao})}(\mathbf{x}) \times \left[ \left( \frac{\epsilon_0(\mathbf{x})}{\epsilon(r_{\text{d}(\text{a})}, \mathbf{x})} \right)^2 - 1 \right] = - [\Delta\sigma(r_{\text{d}(\text{a})}, \mathbf{x})]_{\text{n}(\text{p})}$$

Therefore, one obtains the expressions for relative dielectric constant  $\epsilon(r_{\text{d}(\text{a})}, \mathbf{x})$  and energy band gap  $E_{\text{gn}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x})$ , as:

(i)-for  $r_{\text{d}(\text{a})} \geq r_{\text{do}(\text{ao})}$ , since  $\epsilon(r_{\text{d}(\text{a})}, \mathbf{x}) = \frac{\epsilon_0(\mathbf{x})}{\sqrt{1 + \left[ \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 - 1 \right] \times \ln \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3}} \leq \epsilon_0(\mathbf{x})$ , being a **new**

$\epsilon(r_{\text{d}(\text{a})}, \mathbf{x})$ -law,

$$E_{\text{gno}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d}(\text{a})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{do}(\text{ao})}(\mathbf{x}) = E_{\text{do}(\text{ao})}(\mathbf{x}) \times \left[ \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 - 1 \right] \times \ln \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 \geq 0, \tag{1a}$$

according to the increase in both  $E_{\text{gn}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x})$  and  $E_{\text{d}(\text{a})}(r_{\text{d}(\text{a})}, \mathbf{x})$ , with increasing  $r_{\text{d}(\text{a})}$  and for a given  $\mathbf{x}$ , and

(ii)-for  $r_{\text{d}(\text{a})} \leq r_{\text{do}(\text{ao})}$ , since  $\epsilon(r_{\text{d}(\text{a})}, \mathbf{x}) = \frac{\epsilon_0(\mathbf{x})}{\sqrt{1 - \left[ \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 - 1 \right] \times \ln \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3}} \geq \epsilon_0(\mathbf{x})$ , with a

condition, given by:  $\left[ \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 - 1 \right] \times \ln \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 < 1$ , being a **new**  $\epsilon(r_{\text{d}(\text{a})}, \mathbf{x})$ -law,

$$E_{\text{gno}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d}(\text{a})}(r_{\text{d}(\text{a})}, \mathbf{x}) - E_{\text{do}(\text{ao})}(\mathbf{x}) = -E_{\text{do}(\text{ao})}(\mathbf{x}) \times \left[ \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 - 1 \right] \times \ln \left( \frac{r_{\text{d}(\text{a})}}{r_{\text{do}(\text{ao})} \right)^3 \leq 0, \tag{1b}$$

corresponding to the decrease in both  $E_{\text{gn}(\text{gp})}(r_{\text{d}(\text{a})}, \mathbf{x})$  and  $E_{\text{d}(\text{a})}(r_{\text{d}(\text{a})}, \mathbf{x})$ , with decreasing  $r_{\text{d}(\text{a})}$  and for a given  $\mathbf{x}$ ; therefore, the effective Bohr radius  $a_{\text{Bn}(\text{Bp})}(r_{\text{d}(\text{a})}, \mathbf{x})$  is defined by:

$$a_{\text{Bn}(\text{Bp})}(r_{\text{d}(\text{a})}, \mathbf{x}) \equiv \frac{\epsilon(r_{\text{d}(\text{a})}, \mathbf{x}) \times \hbar^2}{m_{\text{c}(\text{v})}(\mathbf{x}) \times m_0 \times q^2} = 0.53 \times 10^{-8} \text{ cm} \times \frac{\epsilon(r_{\text{d}(\text{a})}, \mathbf{x})}{m_{\text{c}(\text{v})}(\mathbf{x})}. \tag{2}$$

### Generalized Mott Criterium in the Metal-Insulator Transition

Furthermore, it is interesting to remark that the critical total donor (acceptor)-density in the metal-insulator transition (MIT) at  $T=0$  K,  $N_{\text{CDn}(\text{NDp})}(r_{\text{d}(\text{a})}, \mathbf{x})$ , was given by the Mott's criterium, with an empirical parameter,  $M_{\text{n}(\text{p})}$ , as:

$$N_{CDn(CDp)}(r_{d(a)}, x)^{1/3} \times a_{Bn(Bp)}(r_{d(a)}, x) = M_{n(p)}, M_{n(p)} = 0.25, \quad (3)$$

depending thus on our **new**  $\varepsilon(r_{d(a)}, x)$ -law.

This excellent one can be explained from the definition of the reduced effective Wigner-Seitz (WS) radius  $r_{sn(sp)}$ , characteristic of interactions, by:

$$r_{sn(sp)}(N, r_{d(a)}, x) \equiv \left(\frac{3}{4\pi N}\right)^{1/3} \times \frac{1}{a_{Bn(Bp)}(r_{d(a)}, x)} = 1.1723 \times 10^8 \times \left(\frac{1}{N}\right)^{1/3} \times \frac{m_{c(v)}(x) \times m_0}{\varepsilon(r_{d(a)}, x)}, \quad (4)$$

being equal to, in particular, at  $N=N_{CDn(CDp)}(r_{d(a)}, x)$ :  $r_{sn(sp)}(N_{CDn(CDp)}(r_{d(a)}, x), r_{d(a)}, x) = 2.4813963$ , for any  $(r_{d(a)}, x)$ -values. Then, from Eq. (4), one also has :

$$N_{CDn(CDp)}(r_{d(a)}, x)^{1/3} \times a_{Bn(Bp)}(r_{d(a)}, x) = \left(\frac{3}{4\pi}\right)^{1/3} \times \frac{1}{2.4813963} = 0.25 = (WS)_{n(p)} = M_{n(p)}, \quad (5)$$

**explaining thus the existance of the Mott’s criterium**

Furthermore, by using  $M_{n(p)} = 0.25$ , according to the empirical Heisenberg parameter  $\mathcal{H}_{n(p)} = 0.47137$ , as those given in our previous work (Van Cong, 2024), we have also showed that  $N_{CDn(CDp)}$  is just **the density of electrons (holes) localized in the exponential conduction (valence)-band tail,  $N_{CDn(CDp)}^{EBT}$** , with a precision of the order of  $2.86 \times 10^{-7}$ .

It should be noted that the values of  $M_{n(p)}$  and  $\mathcal{H}_{n(p)}$  could be chosen so that those of  $N_{CDn(CDp)}$  and  $N_{CDn(CDp)}^{EBT}$  are in good agreement with their experimental results.

Therefore, the density of electrons (holes) given in parabolic conduction (valence) bands can be defined, as that given in compensated materials, by:

$$N^*(N, r_{d(a)}, x) \equiv N - N_{CDn(NDp)}(r_{d(a)}, x) = N^*, \text{ for a presentation simplicity.} \quad (6)$$

In summary, as observed in Table 1 of our previous paper (Van Cong, 2024), one remarks that, for a given  $x$  and an increasing  $r_{d(a)}$ ,  $\varepsilon(r_{d(a)}, x)$  decreases, while  $E_{gno(gpo)}(r_{d(a)}, x)$ ,  $N_{CDn(NDp)}(r_{d(a)}, x)$  and  $N_{CDn(CDp)}^{EBT}(r_{d(a)}, x)$  increase, affecting strongly all the physical properties, as those observed in following Sections.

**PHYSICAL MODEL**

In the  $n^+(p^+) - p(n) X(x) \equiv InSb_{1-x}As_x$ - crystalline alloy, if denoting the Fermi wave number by:  $k_{Fn(Fp)}(N^*) \equiv \left(\frac{3\pi^2 N^*}{\varepsilon_{c(v)}}\right)^{1/3}$ , the reduced effective Wigner-Seitz (WS) radius  $r_{sn(sp)}$ ,

characteristic of interactions, being given in Eq. (4), in which  $N$  is replaced by  $N^*$ , is now defined by:

$$\gamma \times r_{sn(sp)}(N^*) \equiv \frac{k_{Fn(Fp)}^{-1}}{a_{Bn(Bp)}} < 1,$$

being proportional to  $N^{*-1/3}$ . Here,  $\gamma = (4/9\pi)^{1/3}$ ,  $k_{Fn(Fp)}^{-1}$  means the averaged distance between ionized donors (acceptors), and  $a_{Bn(Bp)}(r_{d(a)}, x)$  is determined in Eq. (2).

Then, the ratio of the inverse effective screening length  $k_{sn(sp)}$  to Fermi wave number  $k_{Fn(kp)}$  at 0 K is defined by:

$$R_{sn(sp)}(N^*) \equiv \frac{k_{sn(sp)}}{k_{Fn(Fp)}} = \frac{k_{Fn(Fp)}^{-1}}{k_{sn(sp)}^{-1}} = R_{snWS(spWS)} + [R_{snTF(spTF)} - R_{snWS(spWS)}]e^{-r_{sn(sp)}} < 1, \quad (7)$$

being valid at any  $N^*$

Here, these ratios,  $R_{snTF(spTF)}$  and  $R_{snWS(spWS)}$ , can be determined as follows.

First, for  $N \gg N_{CDn(NDp)}(r_{d(a)}, x)$ , according to the **Thomas-Fermi (TF)-approximation**, the ratio  $R_{snTF(spTF)}(N^*)$  is reduced to

$$R_{snTF(spTF)}(N^*) \equiv \frac{k_{snTF(spTF)}}{k_{Fn(Fp)}} = \frac{k_{Fn(Fp)}^{-1}}{k_{snTF(spTF)}^{-1}} = \sqrt{\frac{4\gamma r_{sn(sp)}}{\pi}} \ll 1, \quad (8)$$

being proportional to  $N^{*-1/6}$ .

Secondly, for  $N \ll N_{CDn(NDp)}(r_{d(a)})$ , according to the **Wigner-Seitz (WS)-approximation**, the ratio  $R_{snWS(spWS)}$  is respectively reduced to

$$R_{sn(sp)WS}(N^*) \equiv \frac{k_{sn(sp)WS}}{k_{Fn}} = 0.5 \times \left( \frac{s}{2\pi} - \gamma \frac{d[r_{sn(sp)}^2 \times E_{CE}(N^*)]}{dr_{sn(sp)}} \right), \quad (9)$$

where  $E_{CE}(N^*)$  is the majority-carrier correlation energy (CE), being determined by (Van Cong, 2018):

$$E_{CE}(N^*) = \frac{-0.87553}{0.0908 + r_{sn(sp)}} + \frac{\frac{0.87553}{0.0908 + r_{sn(sp)}} + \left(\frac{2[1 - \ln(2)]}{\pi^2}\right) \times \ln(r_{sn(sp)}) - 0.093288}{1 + 0.03847728 \times r_{sn(sp)}^{1.67378876}}.$$

Furthermore, in the highly degenerate case, the physical conditions are found to be given by (Van Cong, 2018)

$$\frac{k_{Fn(Fp)}^{-1}}{a_{Bn(Bp)}} < \frac{\eta_{n(p)}}{E_{Fno(Fpo)}} \equiv \frac{1}{A_{n(p)}} < \frac{k_{Fn(Fp)}^{-1}}{k_{sn(sp)}^{-1}} \equiv R_{sn(sp)} < 1, \quad \eta_{n(p)}(N^*) \equiv \frac{\sqrt{2\pi N^*}}{\varepsilon(r_{d(a)})} \times q^2 k_{sn(sp)}^{-1/2}, \quad (10)$$

which gives:  $A_{n(p)}(N^*) = \frac{E_{Fno(Fpo)}(N^*)}{\eta_{n(p)}(N^*)}$ .

**FERMI ENERGY AND FERMI-DIRAC DISTRIBUTION FUNCTION**

**Fermi Energy and generalized Einstein relation**

Here, for a presentation simplicity, we change all the sign of various parameters, given in the  $p^+ - X(x)$ - crystalline alloy in order to obtain the same one, as given in the  $n^+ - X(x)$ - crystalline alloy, according to the reduced Fermi energy,  $\xi_{n(p)}(N, r_{d(a)}, x, T) \equiv \frac{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}{k_B T} > 0 (< 0)$ , obtained respectively in the degenerate (non-degenerate) case.

For any  $(N, r_{d(a)}, x, T)$ , the reduced Fermi energy  $\xi_{n(p)}(N, r_{d(a)}, x, T)$  or the Fermi energy  $E_{Fn(Fp)}(N, r_{d(a)}, x, T)$ , obtained in our previous paper (Van Cong and Debais, 1993), obtained with a precision of the order of  $2.11 \times 10^{-4}$ , is found to be given by:

$$\xi_{n(p)}(u) \equiv \frac{E_{Fn(Fp)}(u)}{k_B T} = \frac{G(u) + Au^B F(u)}{1 + Au^B} \equiv \frac{V(u)}{W(u)}, A = 0.0005372 \text{ and } B = 4.82842262, \quad (11)$$

where  $u$  is the reduced electron density,  $u(N, r_{d(a)}, x, T) \equiv \frac{N^*}{N_{c(v)}(T, x)}$ ,

$$N_{c(v)}(T, x) = 2g_{c(v)} \times \left( \frac{m_{c(v)}(x) \times m_0 \times k_B T}{2\pi \hbar^2} \right)^{\frac{3}{2}} \text{ (cm}^{-3}\text{)}, \quad g_{c(v)} = 1,$$

$$F(u) = au^{\frac{2}{3}} \left( 1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}} \right)^{-\frac{2}{3}}, a = [(3\sqrt{\pi}/4)]^{2/3}, b = \frac{1}{8} \left( \frac{\pi}{a} \right)^2, c = \frac{62.3739855}{1920} \left( \frac{\pi}{a} \right)^4, \text{ and}$$

$$G(u) \simeq \text{Ln}(u) + 2^{-\frac{8}{3}} \times u \times e^{-du}; d = 2^{3/2} \left[ \frac{1}{\sqrt{27}} - \frac{8}{16} \right] > 0.$$

So, in the non-degenerate case ( $u \ll 1$ ), one has:  $E_{Fn(Fp)}(u) = k_B T \times G(u) \simeq k_B T \times \text{Ln}(u)$  as  $u \rightarrow 0$ , **the limiting condition**, and in the very degenerate case ( $u \gg 1$ ), one gets:

$$E_{Fn(Fp)}(u) = k_B T \times F(u) = k_B T \times au^{\frac{2}{3}} \left( 1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}} \right)^{-\frac{2}{3}} \simeq \frac{\hbar^2 \times k_{Fn(Fp)}^2(N^*)}{2 \times m_{c(v)}(x) \times m_0} \text{ as } u \rightarrow \infty,$$

**the limiting condition.** In other words,  $\xi_{n(p)} \equiv \frac{E_{Fn(Fp)}}{k_B T}$  is accurate, and it also verifies the correct limiting conditions. In the following, it will be present in all the electrical-and-thermoelectric coefficients.

In particular, at  $T=0K$ , since  $u^{-1} = 0$ , Eq. (11) is reduced to:  $E_{Fno(Fpo)}(N^*) \equiv \frac{\hbar^2 \times k_{Fn(Fp)}^2(N^*)}{2 \times m_{c(v)}(x) \times m_0}$ , being proportional to  $(N^*)^{2/3}$ , and also equal to 0, according to the MIT.

In the following, it should be noted that such the accurate expression of  $\xi_{n(p)}(N, r_{d(a)}, x, T)$  is present in all the following electrical-and-thermoelectric.

**FERMI-DIRAC DISTRIBUTION FUNCTION (FDDF)**

The Fermi-Dirac distribution function (FDDF) is given by:  $f(E) \equiv (1 + e^\gamma)^{-1}$ ,  $\gamma \equiv (E - E_{Fn(Fp)})/(k_B T)$ .

So, the average of  $E^p$ , calculated using the FDDF-method, as developed in our previous work (Van Cong, 2018) is found to be given by:

$$\langle E^p \rangle_{FDDF} \equiv G_p(E_{Fn(Fp)}) \times E_{Fn(Fp)}^p \equiv \int_{-\infty}^{\infty} E^p \times \left( -\frac{\partial f}{\partial E} \right) dE, \quad -\frac{\partial f}{\partial E} = \frac{1}{k_B T} \times \frac{e^\gamma}{(1+e^\gamma)^2}.$$

Further, one notes that, at 0 K,  $-\frac{\partial f}{\partial E} = \delta(E - E_{Fn(Fp)})$ ,  $\delta(E - E_{Fn(Fp)})$  being the Dirac delta ( $\delta$ )-function. Therefore,  $G_p(E_{Fn(Fp)}) = 1$ .

Then, at low T, by a variable change  $\gamma \equiv (E - E_{Fn(Fp)})/(k_B T)$ , one has:

$$G_p(E_{Fn(Fp)}) \equiv 1 + E_{Fn(Fp)}^{-p} \times \int_{-\infty}^{\infty} \frac{e^\gamma}{(1+e^\gamma)^2} \times (k_B T \gamma + E_{Fn(Fp)})^p d\gamma = 1 + \sum_{\mu=1,2,\dots}^p C_p^\beta \times (k_B T)^\beta \times E_{Fn(Fp)}^{-\beta} \times I_\beta,$$

where  $C_p^\beta \equiv p(p-1) \dots (p-\beta+1)/\beta!$  and the integral  $I_\beta$  is given by:

$$I_\beta = \int_{-\infty}^{\infty} \frac{\gamma^\beta \times e^\gamma}{(1+e^\gamma)^2} d\gamma = \int_{-\infty}^{\infty} \frac{\gamma^\beta}{(e^{\gamma/2} + e^{-\gamma/2})^2} d\gamma, \text{ vanishing for odd values of } \beta. \text{ Then, for even values of } \beta = 2n, \text{ with } n=1, 2, \dots, \text{ one obtains:}$$

$$I_{2n} = 2 \int_0^{\infty} \frac{\gamma^{2n} \times e^\gamma}{(1+e^\gamma)^2} d\gamma.$$

Now, using an identity  $(1 + e^\gamma)^{-2} \equiv \sum_{s=1}^{\infty} (-1)^{s+1} s \times e^{\gamma(s-1)}$ , a variable change:  $s\gamma = -t$ , the Gamma function:  $\int_0^{\infty} t^{2n} e^{-t} dt \equiv \Gamma(2n + 1) = (2n)!$ , and also the definition of the Riemann's zeta function:  $\zeta(2n) \equiv 2^{2n-1} \pi^{2n} |B_{2n}| / (2n)!$ ,  $B_{2n}$  being the Bernoulli numbers, one finally gets:  $I_{2n} = (2^{2n} - 2) \times \pi^{2n} \times |B_{2n}|$ . So, from Eq. (22), we get in the degenerate case the following ratio:

$$G_p(E_{Fn(Fp)}) \equiv \frac{\langle E^p \rangle_{FDDF}}{E_{Fn(Fp)}^p} = 1 + \sum_{n=1}^p \frac{p(p-1)\dots(p-2n+1)}{(2n)!} \times (2^{2n} - 2) \times |B_{2n}| \times y^{2n} \equiv G_{p \geq 1}(y), \quad (12)$$

where  $y \equiv \frac{\pi}{\xi_{n(p)}(N^*, T)} = \frac{\pi k_B T}{E_{Fn(Fp)}(N^*, T)}$ .



Then, some usual results of  $G_{p \geq 1}(y)$  are given in **Table 2 in Appendix 1, being important ones in this work.**

**ELECTRICAL-AND-THERMOELECTRIC PROPERTIES**

Here, if denoting, for majority electrons (holes), the electrical conductivity by  $\sigma(N, r_{d(a)}, x, T)$ , expressed in  $\text{ohm}^{-1} \times \text{cm}^{-1}$ , the thermal conductivity by  $\kappa(N, r_{d(a)}, x, T)$ , expressed in  $\frac{\text{W}}{\text{cm} \times \text{K}}$ , and Lorenz number  $L$  by:

$L = \frac{\pi^2}{3} \times \left(\frac{k_B}{q}\right)^2 = 2.4429637 \left(\frac{\text{W} \times \text{ohm}}{\text{K}^2}\right) = 2.4429637 \times 10^{-8} (\text{V}^2 \times \text{K}^{-2})$ , then the well-known Wiedemann-Frank law states that the ratio,  $\frac{\kappa}{\sigma}$ , is proportional to the temperature  $T(\text{K})$ , as:

$$\frac{\kappa(N, r_{d(a)}, x, T)}{\sigma(N, r_{d(a)}, x, T)} = L \times T. \tag{13}$$

We now determine the general form of  $\sigma$  in the following.

First, it is expressed in terms of the kinetic energy of the electron (hole),  $E_k \equiv \frac{\hbar^2 \times k^2}{2 \times m_{Cn(Cp)} \times m_0}$ , or the wave number  $k$ , as:

$$\sigma(k) \equiv \frac{q^2 \times k}{\pi \times \hbar} \times \frac{k}{k_{sn(sp)}} \times [k \times a_{Bn(Bp)}] \times \left(\frac{E_k}{\eta_{n(p)}}\right)^{1/2},$$

which is thus proportional to  $E_k^2$ .

Then, for  $E \geq 0$ , we obtain:  $\langle E^2 \rangle_{FDDF} \equiv G_2(y = \frac{\pi k_B T}{E_{Fn(Fp)}}) \times E_{Fn(Fp)}^2$ , and  $G_2(y) = \left(1 + \frac{y^2}{3}\right) \equiv G_2(N, r_{d(a)}, x, T)$ , with  $y \equiv \frac{\pi}{\xi_{n(p)}}$ ,  $\xi_{n(p)} = \xi_{n(p)}(N, r_{d(a)}, x, T)$  for a presentation simplicity. Therefore, one obtains:

$$\sigma(N, r_{d(a)}, x, T) \equiv \left[ \frac{q^2}{\pi \times \hbar} \times \frac{k_{Fn(Fp)}(N^*)}{R_{sn(sp)}(N^*)} \times [k_{Fn(Fp)}(N^*) \times a_{Bn(Bp)}(r_{d(a)})] \times \sqrt{A_{n(p)}(N^*)} \right] \times \left[ G_2(N, r_{d(a)}, x, T) \times \left(\frac{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}{E_{Fno(Fpo)}(N^*)}\right)^2 \right] \left(\frac{1}{\text{ohm} \times \text{cm}}\right),$$

$$\frac{q^2}{\pi \times \hbar} = 7.7480735 \times 10^{-5} \text{ ohm}^{-1}, A_{n(p)}(N^*) = \frac{E_{Fno(Fpo)}(N^*)}{\eta_{n(p)}(N^*)}, \tag{14}$$

which also determine the resistivity as:  $\rho(N, r_{d(a)}, x, T) \equiv 1/\sigma(N, r_{d(a)}, x, T)$ , noting that  $N^* \equiv N - N_{CDn(NDp)}(r_{d(a)}, x)$ . **This  $\sigma(N, r_{d(a)}, x, T)$ -result is an essential one in this paper.**

In Eq. (14), one notes that at  $T=0\text{ K}$ ,  $\sigma(N, r_{d(a)}, x, T = 0\text{K})$  is proportional to  $E_{Fno(Fpo)}^{\frac{3}{2}}$ , or to  $N^*$ . Thus,  $\sigma(N = N_{CDn(NDp)}, r_{d(a)}, x, T = 0\text{K}) = 0$  at  $N^* = 0$ , at which the metal-insulator transition (MIT) occurs.

**Electrical Coefficients**

The relaxation time  $\tau$  is related to  $\sigma$  by:

$$\tau(N, r_{d(a)}, x, T) \equiv \sigma(N, r_{d(a)}, x, T) \times \frac{m_{c(v)}(x) \times m_0}{q^2 \times N^*}. \text{ Therefore, the mobility } \mu \text{ is given by:}$$

$$\mu(N, r_{d(a)}, x, T) \equiv \mu(N^*, r_{d(a)}, T) = \frac{q \times \tau(N, r_{d(a)}, x, T)}{m_{c(v)}(x) \times m_0} = \frac{\sigma(N, r_{d(a)}, x, T)}{q \times N^*} \left( \frac{\text{cm}^2}{\text{V} \times \text{s}} \right). \tag{15}$$

Here, at  $T=0\text{K}$ ,  $\mu(N^*, r_{d(a)}, T)$  is thus proportional to  $(N^*)^{1/3}$ , since  $\sigma(N^*, r_{d(a)}, T = 0\text{K})$  is proportional to  $(N^*)^{4/3}$ . Thus,  $\mu(N^* = 0, r_{d(a)}, T = 0\text{K}) = 0$  at  $N^* = 0$ , at which the metal-insulator transition (MIT) occurs.

Then, since  $\tau$  and  $\sigma$  are both proportional to  $E_{Fn(Fp)}(N^*, T)^2$ , as given above, the Hall factor can thus be determined by:

$$r_H(N, r_{d(a)}, x, T) \equiv \frac{(\tau^2)_{FDDF}}{[(\tau)_{FDDF}]^2} = \frac{G_4(y)}{[G_2(y)]^2}, y \equiv \frac{\pi}{\xi_{n(p)}(N, r_{d(a)}, x, T)} = \frac{\pi k_B T}{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}, \text{ and therefore,}$$

the Hall mobility yields:

$$\mu_H(N, r_{d(a)}, x, T) \equiv \mu(N, r_{d(a)}, x, T) \times r_H(N^*, T) \left( \frac{\text{cm}^2}{\text{V} \times \text{s}} \right), \tag{16}$$

noting that, at  $T=0\text{K}$ , since  $r_H(N, r_{d(a)}, x, T) = 1$ , one then gets at  $N = N_{CDn(NDp)}$ :

$$\mu_H(N, r_{d(a)}, x, T) \equiv \mu(N, r_{d(a)}, x, T) = 0 \text{ at } N^* = 0, \text{ at which the metal-insulator transition (MIT) occurs.}$$

Finally, the **generalized Einstein relation** is found to be defined (Van Cong, 1980) as:

$$\frac{D(N, r_{d(a)}, x, T)}{\mu(N, r_{d(a)}, x, T)} \equiv \frac{N}{q} \times \frac{dE_{Fn(Fp)}}{dN} \equiv \frac{k_B \times T}{q} \times \left( u \frac{d\xi_{n(p)}(u)}{du} \right),$$

where  $D(N^*, r_{d(a)}, T)$  is the diffusion coefficient,  $\xi_{n(p)}(u)$  is defined in Eq. (11), and the mobility  $\mu(N, r_{d(a)}, x, T)$  is determined in Eq. (15). Then, by differentiating this function  $\xi_{n(p)}(u)$  with respect to  $u$ , one thus obtains  $\frac{d\xi_{n(p)}(u)}{du}$ . Therefore,

$$\frac{D(N^*, r_{d(a)}, T)}{\mu(N^*, r_{d(a)}, T)} = \frac{k_B \times T}{q} \times u \frac{V'(u) \times W(u) - V(u) \times W'(u)}{W^2(u)}, \tag{17}$$

where  $W'(u) = ABu^{B-1}$  and

$$V'(u) = u^{-1} + 2^{-\frac{3}{2}} e^{-du} (1 - du) + \frac{2}{3} Au^{B-1} F(u) \left[ \left(1 + \frac{3B}{2}\right) + \frac{4}{3} \times \frac{bu^{-\frac{4}{3}} + 2cu^{-\frac{8}{3}}}{1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}}} \right].$$

One remarks that: (i) as  $u \rightarrow 0$ , one has:  $W^2 \simeq 1$  and  $u[V' \times W - V \times W'] \simeq 1$ , and therefore:

$$\frac{D_{n(p)}(u)}{\mu} \simeq \frac{k_B \times T}{q}, \quad \text{and} \quad \text{(ii) as } u \rightarrow \infty, \quad \text{one has: } W^2 \approx A^2 u^{2B} \quad \text{and}$$

$u[V' \times W - V \times W'] \approx \frac{2}{3} au^{2/3} A^2 u^{2B}$ , and therefore, in this **highly degenerate case** and at

$T=0K$ , the **above generalized Einstein relation** is reduced to the **usual Einstein one**:

$$\frac{D(N^*, r_{d(a)}, T=0)}{\mu(N^*, r_{d(a)}, T=0)} \approx \frac{2}{3} E_{Fno(Fpo)}(N^*)/q.$$

In other words, **Eq. (17) verifies the correct limiting conditions.**

One also notes that, for  $N^* = 0$ ,  $\mu(N^* = 0, r_{d(a)}, T = 0K) = 0$ , as remarked in above, and therefore, for any  $r_{d(a)}$ ,  $D(N^* = 0, r_{d(a)}, T = 0K) = 0$ , according to the MIT.

Further, in the present degenerate case ( $u \gg 1$ ), Eq. (17) gives:

$$\frac{D(N, r_{d(a)}, x, T)}{\mu(N, r_{d(a)}, x, T)} \simeq \frac{2}{3} \times \frac{E_{Fno(Fpo)}(u)}{q} \times \left[ 1 + \frac{4}{3} \times \frac{\left(bu^{-\frac{4}{3}} + 2cu^{-\frac{8}{3}}\right)}{\left(1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}}\right)} \right], \tag{18}$$

where  $a = [(3\sqrt{\pi}/4)]^{2/3}$ ,  $b = \frac{1}{8} \left(\frac{\pi}{a}\right)^2$  and  $c = \frac{62.3739855}{1920} \left(\frac{\pi}{a}\right)^4$ .

In **Tables 3n(3p) given in Appendix 1**, for given  $x$ ,  $N$  and  $T(=4.2 K$  and  $77 K)$ , and from Equations (14, 15, 16, 18), the numerical results of the coefficients:  $\sigma, \mu, \mu_H, D$ , expressed respectively in  $\left(\frac{10^8}{ohm \times cm}, \frac{10^8 \times cm^2}{V \times s}, \frac{10^8 \times cm^2}{V \times s}, \frac{10 \times cm^2}{s}\right)$ , are found to be decreased with increasing  $r_{d(a)}$ , respectively.

**Thermoelectric Coefficients**

First off all, from Eq. (14), obtained for  $\sigma(N, r_{d(a)}, x, T)$ , the well-known Mott definition for the thermoelectric power or for the Seebeck coefficient,  $S$ , is given by:

$$S(N, r_{d(a)}, x, T) \equiv \frac{-\pi^2}{3} \times \frac{k_B}{q_{>0}} \times k_B T \times \left. \frac{\partial \ln \sigma(E)}{\partial E} \right]_{E=E_{Fn(Fp)}} = \frac{-\pi^2}{3} \times \frac{k_B}{q} \times \frac{\partial \ln \sigma(\xi_{n(p)})}{\partial \xi_{n(p)}}.$$

Then, using Eq. (11), for  $\xi_{n(p)}(N, r_{d(a)}, x, T) \gtrsim 1$ , one gets, by putting

$$F_S(N, r_{d(a)}, x, T) \equiv \left[ 1 - \frac{y^2}{3 \times G_2 \left( y = \frac{\pi}{\xi_{n(p)}} \right)} \right],$$

$$S(N, r_{d(a)}, x, T) \equiv \frac{-\pi^2}{3} \times \frac{k_B}{q} \times \frac{2F_{Sb}(N^*, T)}{\xi_{n(p)}} = -\sqrt{\frac{3 \times L}{\pi^2}} \times \frac{2 \times \xi_{n(p)}}{\left( 1 + \frac{3 \times \xi_{n(p)}^2}{\pi^2} \right)} \left( \frac{V}{K} \right), \quad (19)$$

giving here: (i) at  $\xi_{n(p)} = \sqrt{\frac{\pi^2}{3}} \simeq 1.8138$ , one gets:  $S = -\sqrt{L} \simeq -1.563 \times 10^{-4} \left( \frac{V}{K} \right)$  and at  $\xi_{n(p)} = 1$  one obtains:  $S \simeq -1.322 \times 10^{-4} \left( \frac{V}{K} \right)$ .

Further, the figure of merit, ZT, is found to be given by:

$$ZT(N, r_{d(a)}, x, T) \equiv \frac{S^2 \times \sigma \times T}{\kappa} = \frac{S^2}{L} = (ZT)_{Mott} \times [2 \times F_S]^2, \quad (ZT)_{Mott} = \frac{\pi^2}{3 \times \xi_{n(p)}^2}, \quad (20)$$

giving here: (i) at  $\xi_{n(p)} = \sqrt{\frac{\pi^2}{3}} \simeq 1.8138$ , one gets:  $ZT = (ZT)_{Mott} = 1$ , and at  $\xi_{n(p)} = 1$  one obtains:  $ZT \simeq 0.715$  and  $(ZT)_{Mott} = \frac{\pi^2}{3} \simeq 3.290$ .

Furthermore, from Eq. (19), one gets:

$$\frac{\partial S}{\partial \xi_{n(p)}} = \sqrt{\frac{3 \times L}{\pi^2}} \times \frac{\frac{3 \times \xi_{n(p)}^2}{\pi^2} - 1}{\left( 1 + \frac{3 \times \xi_{n(p)}^2}{\pi^2} \right)^2}, \quad \frac{dS}{dT} = \frac{\partial S}{\partial \xi_{n(p)}} \times \frac{\partial \xi_{n(p)}}{\partial T}, \quad \text{and} \quad \frac{dS}{dN} = \frac{\partial S}{\partial \xi_{n(p)}} \times \frac{\partial \xi_{n(p)}}{\partial N}, \quad \text{and}$$

$$\frac{d(ZT)}{dT} = \frac{2 \times S}{L} \times \frac{dS}{dT} \quad \text{and} \quad \frac{d(ZT)}{dN} = \frac{2 \times S}{L} \times \frac{dS}{dN}, \quad (21)$$

noting that: (i) at given  $(N, r_{d(a)}, x)$ , and for  $\frac{\partial \xi_{n(p)}}{\partial T} > 0$  (or  $< 0$ ),  $\xi_{n(p)}$  increases (or decreases) for decreasing (or increasing) T, (ii) at given  $(r_{d(a)}, x, T)$ , and for  $\frac{\partial \xi_{n(p)}}{\partial N} > 0$  (or  $< 0$ ),  $\xi_{n(p)}$  increases (or decreases) for increasing (or decreasing) N.

Finally, the Van-Cong coefficient, VC, is given by:

$$VC(N, r_{d(a)}, x, T) \equiv N \times \frac{dS}{dN} \left( \frac{V}{K} \right), \quad (22)$$

the Thomson coefficient, Ts, by:

$$Ts(N, r_{d(a)}, x, T) \equiv T \times \frac{dS}{dT} \left( \frac{V}{K} \right), \quad (23)$$

and then, the Peltier coefficient,  $P_t$ , as:

$$P_t(N, r_{d(a)}, x, T) \equiv T \times S \text{ (V)}. \quad (24)$$

Now, in the lightly degenerate n(p)-type  $\text{InSb}_{1-x}\text{As}_x$  alloy, in which  $N=5 \times 10^{17} \text{ cm}^{-3}$  ( $5 \times 10^{18} \text{ cm}^{-3}$ ), and for  $T=3\text{K}$  and  $80\text{K}$ , the numerical results of various thermoelectric coefficients are reported in Tables 4n(4p) in Appendix 1, noting that their variations with increasing  $r_{d(a)}$  are represented by the arrows: ↗ (increase), and ↘ (decrease), respectively.

Then, in Tables 5n(5p) given Appendix 1 for a given  $N$  and with increasing  $T$ , and then in Tables 6n(6p) given Appendix 1 for a given  $T$  and with decreasing  $N$ , the reduced Fermi-energy  $\xi_{n(p)}$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘).

One notes here that with increasing  $T$  (or with decreasing  $N$ ) one obtains: (i) for  $\xi_{n(p)} \simeq 1.8138$ , while the numerical results of  $S$  present a same minimum  $(S)_{\min.} \left( \simeq -1.563 \times 10^{-4} \frac{\text{V}}{\text{K}} \right)$ , those of  $ZT$  show a same maximum  $(ZT)_{\max.} = 1$ , (ii) for  $\xi_{n(p)} = 1$ , those of  $S$ ,  $ZT$ ,  $(ZT)_{\text{Mott}}$ ,  $VC$ , and  $T_s$  present the same results:  $-1.322 \times 10^{-4} \frac{\text{V}}{\text{K}}$ ,  $0.715$ ,  $3.290$ ,  $-1.105 \times 10^{-4} \frac{\text{V}}{\text{K}}$ , and  $1.657 \times 10^{-4} \frac{\text{V}}{\text{K}}$ , respectively, and (iii) for  $\xi_n \simeq 1.8138$ ,  $(ZT)_{\text{Mott}} = 1$ . It seems that these results could present a new law in the thermoelectric properties, obtained in the degenerate case.

### CONCLUDING REMARKS

In the  $n^+(p^+) - p(n)$   $\text{InSb}_{1-x}\text{As}_x$ - crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018), were revised and performed, by basing on our following basic expressions.

(1) The effective extrinsic static dielectric constant law,  $\varepsilon(r_{d(a)}, x)$ , due to the impurity size effect, is determined in Eq. (1).

(2) The generalized Mott criterium in the metal-insulator transition is expressed in Equations (3, 5, 6), showing that  $N_{\text{CDn(CDp)}}$  is just the density of electrons (holes) localized in the exponential conduction (valence)-band tail,  $N_{\text{CDn(CDp)}}^{\text{EBT}}$ , with a precision of the order of  $2.86 \times 10^{-7}$ , as given in our recent work (Van Cong, 2024), and the effective electron

(hole)-density:  $N^* \equiv N - N_{CDn(CDp)} \simeq N - N_{CDn(CDp)}^{EBT}$ , as that observed in the compensated crystals.

(3) The ratio of the inverse effective screening length  $k_{sn(sp)}$  to Fermi wave number  $k_{Fn(kp)}$  at 0 K,  $R_{sn(sp)}(N^*)$ , defined in Eq. (7), is valid at any density  $N^*$ .

(4) The Fermi energy for any  $N$  and  $T$ ,  $E_{Fn(Fp)}$ , determined in Eq. (11) with a precision of the order of  $2.11 \times 10^{-4}$  (Van Cong, 1993), and it exists in all the expressions of electrical-and-thermoelectric coefficients.

(5) Our expressions for the electrical conductivity,  $\sigma$ , and for the Seebeck coefficient,  $S$ , determined respectively in Equations (14, 19) are the basic expressions for determining the electrical-and-thermoelectric coefficients.

(6) Finally, in Tables 5n(5p) given Appendix 1 for a given  $N$  and with increasing  $T$ , and then in Tables 6n(6p) given Appendix 1 for a given  $T$  and with decreasing  $N$ , the reduced Fermi-energy  $\xi_{n(p)}$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing  $T$  (or with decreasing  $N$ ) one obtains: (i) for  $\xi_{n(p)} \simeq 1.8138$ , while the numerical results of  $S$  present a **same minimum**  $(S)_{min.} (\simeq -1.563 \times 10^{-4} \frac{V}{K})$ , those of  $ZT$  show a **same maximum**  $(ZT)_{max.} = 1$ , (ii) for  $\xi_{n(p)} = 1$ , those of  $S$ ,  $ZT$ ,  $(ZT)_{Mott}$ ,  $VC$ , and  $T_s$  present **the same results**:  $-1.322 \times 10^{-4} \frac{V}{K}$ ,  $0.715$ ,  $3.290$ ,  $-1.105 \times 10^{-4} \frac{V}{K}$ , and  $1.657 \times 10^{-4} \frac{V}{K}$ , respectively, and (iii) for  $\xi_n \simeq 1.8138$ ,  $(ZT)_{Mott} = 1$ . It seems that these results could present a new law in the thermoelectric properties, obtained in the degenerate case.

In summary, all the numerical results of electrical-and-thermoelectric coefficients, given in our previous work (Van Cong, 2018), are now revised and performed.

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APPENDIX 1

**Table 1:** The values of various energy-band-structure parameters are given in various crystalline alloys as follows.

In  $InSb_{1-x}As_x$ -alloy, in which  $r_{do(As)} = r_{Sb(M)} = 0.136$  nm (0.144 nm), we have:  $g_{c(v)}(x) = 1 \times x + 1 \times (1 - x)$ ,  $m_{c(v)}(x)/m_0 = 0.09 (0.3) \times x + 0.1 (0.4) \times (1 - x)$ ,  $\epsilon_0(x) = 14.55 \times x + 16.9 \times (1 - x)$ ,  $E_{go}(x) = 0.43 \times x + 0.23 \times (1 - x)$ .

**Table 2:** Expressions for  $G_{p \geq 1}(y \equiv \frac{\pi}{\xi_{n(p)}})$ , due to the Fermi-Dirac distribution function, noting that  $G_{p=1}(y \equiv \frac{\pi k_B T}{E_{Fn(Fp)}} = \frac{\pi}{\xi_{n(p)}}) = 1$ , used to determine the electrical-and-thermoelectric coefficients.

$G_{3/2}(y)$	$G_2(y)$	$G_{5/2}(y)$	$G_3(y)$	$G_{7/2}(y)$	$G_4(y)$	$G_{9/2}(y)$
$(1 + \frac{y^2}{8} + \frac{7y^4}{640})$	$(1 + \frac{y^2}{3})$	$(1 + \frac{5y^2}{8} - \frac{7y^4}{384})$	$(1 + y^2)$	$(1 + \frac{35y^2}{24} + \frac{49y^4}{384})$	$(1 + 2y^2 + \frac{7y^4}{15})$	$(1 + \frac{21y^2}{8} + \frac{147y^4}{128})$

**Table 3n:** Here, one notes that, for given x, N and T(=4.2 K and 77 K), the functions:  $\sigma, \mu, \mu_H, D$ , expressed respectively in  $(\frac{10^3}{ohm \times cm}, \frac{10^3 \times cm^2}{V \times s}, \frac{10^3 \times cm^2}{V \times s}, \frac{10^2 \times cm^2}{s})$ , decrease with increasing  $r_d$ .

Donor	P	As	Sb	Sn
$r_d$ (nm)	↗ 0.110	0.118	0.136	0.140

For x=0, the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

N ( $10^{18} \text{ cm}^{-3}$ )

3	1.69, 3.525, 3.526, 1.78	1.48, 3.098, 3.099, 1.56	1.33, 2.793, 2.794, 1.40	1.32, 2.779, 2.780, 1.40
10	4.39, 2.745, 2.746, 3.09	3.82, 2.387, 2.388, 2.69	3.41, 2.136, 2.136, 2.41	3.40, 2.124, 2.124, 2.39
40	14.0, 2.185, 2.185, 6.21	12.0, 1.874, 1.874, 5.33	10.6, 1.658, 1.658, 4.71	10.5, 1.648, 1.648, 4.68
70	22.7, 2.026, 2.026, 8.36	19.4, 1.730, 1.730, 7.14	17.1, 1.524, 1.524, 6.29	17.0, 1.515, 1.515, 6.25

For x=0.5, the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

N ( $10^{18} \text{ cm}^{-3}$ )

3	1.76, 3.686, 3.687, 1.95	1.54, 3.236, 2.237, 1.71	1.39, 2.915, 2.916, 1.54	1.38, 2.900, 2.901, 1.53
10	4.63, 2.891, 2.891, 3.43	4.01, 2.509, 2.510, 2.98	3.58, 2.241, 2.242, 2.66	3.56, 2.230, 2.230, 2.64
40	14.9, 2.321, 2.321, 6.94	12.7, 1.988, 1.988, 5.95	11.2, 1.756, 1.756, 5.25	11.1, 1.745, 1.745, 5.22
70	24.2, 2.159, 2.159, 9.38	20.6, 1.841, 1.841, 8.00	18.1, 1.620, 1.620, 7.04	18.0, 1.609, 1.609, 6.99

For x=1, the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

N ( $10^{18} \text{ cm}^{-3}$ )



3	1.87, 3.905, 3.906, 2.19	1.63, 3.421, 3.422, 1.91	1.47, 3.078, 3.079, 1.72	1.46, 3.062, 3.063, 1.71
10	4.95, 3.091, 3.092, 3.87	4.28, 2.677, 2.677, 3.35	3.81, 2.386, 2.387, 2.99	3.79, 2.373, 2.374, 2.97
40	16.1, 2.508, 2.508, 7.92	13.7, 2.144, 2.144, 6.77	12.1, 1.890, 1.890, 5.97	12.0, 1.879, 1.879, 5.93
70	26.2, 2.341, 2.341, 10.7	22.3, 1.992, 1.992, 9.14	19.6, 1.750, 1.750, 8.03	19.5, 1.739, 1.739, 7.97

For  $x=0$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.74, 3.630, 3.930, 1.85	1.52, 3.191, 3.499, 1.62	1.37, 2.877, 3.155, 1.46	1.36, 2.862, 3.139, 1.45
10	4.42, 2.762, 2.817, 3.12	3.84, 2.402, 2.450, 2.71	3.43, 2.149, 2.192, 2.42	3.42, 2.137, 2.180, 2.41
40	14.0, 2.187, 2.194, 6.22	12.0, 1.876, 1.882, 5.33	10.6, 1.660, 1.665, 4.72	10.6, 1.650, 1.655, 4.69
70	22.7, 2.027, 2.030, 8.37	19.4, 1.731, 1.734, 7.15	17.1, 1.525, 1.527, 6.29	17.0, 1.516, 1.518, 6.26

For  $x=0.5$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.81, 3.785, 4.116, 2.02	1.59, 3.323, 3.614, 1.78	1.43, 2.993, 3.256, 1.60	1.42, 2.978, 3.240, 1.59
10	4.65, 2.907, 2.960, 3.45	4.03, 2.523, 2.569, 3.00	3.60, 2.254, 2.295, 2.68	3.58, 2.242, 2.282, 2.66
40	14.9, 2.323, 2.329, 6.95	12.7, 1.990, 1.995, 5.95	11.2, 1.757, 1.763, 5.26	11.2, 1.747, 1.752, 5.23
70	24.2, 2.160, 2.163, 9.39	20.6, 1.842, 1.844, 8.00	18.2, 1.620, 1.622, 7.04	18.0, 1.610, 1.612, 7.00

For  $x=1$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.91, 3.999, 4.315, 2.26	1.67, 3.504, 3.782, 1.97	1.50, 3.153, 3.403, 1.77	1.49, 3.137, 3.385, 1.76
10	4.97, 3.107, 3.157, 3.90	4.30, 2.690, 2.734, 3.37	3.83, 2.398, 2.438, 3.01	3.81, 2.385, 2.424, 2.99
40	16.1, 2.510, 2.516, 7.93	13.7, 2.145, 2.151, 6.77	12.1, 1.892, 1.896, 5.97	12.0, 1.880, 1.885, 5.94
70	26.3, 2.342, 2.345, 10.7	22.3, 1.993, 1.996, 9.14	19.6, 1.751, 1.753, 8.03	19.5, 1.740, 1.742, 7.98

**Table 3p:** Here, one notes that, for given  $x$ ,  $N$  and  $T(=4.2 \text{ K}$  and  $77 \text{ K})$ , the functions:  $\sigma, \mu, \mu_H, D$ , expressed respectively in  $(\frac{10^8}{\text{ohm}\times\text{cm}}, \frac{10^8 \times \text{cm}^2}{\text{V}\times\text{s}}, \frac{10^8 \times \text{cm}^2}{\text{V}\times\text{s}}, \frac{10 \times \text{cm}^2}{\text{s}})$ , decrease with increasing  $r_a$ .

Acceptor	Ga	Mg	In	Sn
$r_a$ (nm)	↗ 0.120	0.140	0.144	0.148

For  $x=0$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

$N (10^{18} \text{ cm}^{-3})$

3	0.47, 1.598, 1.613, 1.47	0.37, 1.460, 1.477, 1.21	0.37, 1.454, 1.470, 1.20	0.36, 1.448, 1.464, 1.19
10	1.92, 1.356, 1.358, 3.53	1.67, 1.210, 1.211, 3.09	1.65, 1.203, 1.204, 3.06	1.64, 1.196, 1.197, 3.04
40	7.52, 1.209, 1.209, 8.43	6.63, 1.072, 1.072, 7.44	6.58, 1.065, 1.065, 7.39	6.54, 1.058, 1.059, 7.34
70	12.8, 1.164, 1.164, 11.9	11.3, 1.031, 1.031, 10.5	11.2, 1.024, 1.024, 10.4	11.2, 1.018, 1.018, 10.3

For  $x=0.5$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

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 $N (10^{18} \text{ cm}^{-3})$

3	0.57, 1.732, 1.743, 1.94	0.46, 1.574, 1.585, 1.64	0.45, 1.566, 1.577, 1.63	0.45, 1.559, 1.570, 1.61
10	2.15, 1.484, 1.485, 4.48	1.87, 1.323, 1.325, 3.93	1.86, 1.316, 1.317, 3.90	1.85, 1.308, 1.309, 3.88
40	8.28, 1.324, 1.324, 10.6	7.30, 1.173, 1.173, 9.35	7.26, 1.166, 1.166, 9.29	7.21, 1.159, 1.159, 9.23
70	14.1, 1.275, 1.275, 14.9	12.4, 1.129, 1.129, 13.2	12.3, 1.122, 1.122, 13.1	12.2, 1.114, 1.114, 13.0

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 For  $x=1$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 4.2K

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 $N (10^{18} \text{ cm}^{-3})$

3	0.69, 1.924, 1.931, 2.68	0.58, 1.740, 1.747, 2.30	0.57, 1.731, 1.739, 2.29	0.57, 1.722, 1.730, 2.27
10	2.46, 1.661, 1.662, 5.93	2.16, 1.481, 1.482, 5.22	2.14, 1.472, 1.473, 5.19	2.13, 1.463, 1.464, 5.16
40	9.32, 1.482, 1.482, 13.9	8.23, 1.314, 1.314, 12.3	8.18, 1.306, 1.306, 12.2	8.12, 1.298, 1.298, 12.1
70	15.8, 1.427, 1.427, 19.5	14.0, 1.264, 1.264, 17.2	13.9, 1.256, 1.256, 17.1	13.8, 1.248, 1.248, 17.0

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 For  $x=0$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77K

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 $N (10^{18} \text{ cm}^{-3})$

3	0.27, 0.909, 2.709, 0.65	0.18, 0.694, 2.251, 0.41	0.17, 0.682, 2.226, 0.40	0.16, 0.671, 2.199, 0.39
10	2.12, 1.498, 1.978, 4.04	1.85, 1.341, 1.785, 3.55	1.83, 1.333, 1.775, 3.53	1.82, 1.326, 1.766, 3.50
40	7.64, 1.228, 1.291, 8.60	6.73, 1.088, 1.145, 7.59	6.69, 1.082, 1.138, 7.54	6.64, 1.075, 1.131, 7.49
70	12.9, 1.173, 1.201, 12.0	11.4, 1.038, 1.064, 10.6	11.3, 1.032, 1.057, 10.5	11.2, 1.025, 1.051, 10.4

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 For  $x=0.5$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77K

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 $N (10^{18} \text{ cm}^{-3})$

3	0.43, 1.318, 3.226, 1.31	0.32, 1.087, 2.865, 0.96	0.31, 1.075, 2.847, 0.95	0.31, 1.063, 2.828, 0.93
10	2.32, 1.603, 2.001, 4.97	2.03, 1.433, 1.798, 4.38	2.02, 1.425, 1.789, 4.35	2.00, 1.417, 1.779, 4.32
40	8.38, 1.339, 1.392, 10.7	7.39, 1.187, 1.235, 9.49	7.34, 1.180, 1.227, 9.43	7.29, 1.173, 1.220, 9.37
70	14.2, 1.282, 1.306, 15.0	12.5, 1.135, 1.156, 13.3	12.4, 1.128, 1.149, 13.2	12.3, 1.121, 1.142, 13.1

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 For  $x=1$ , the values of  $(\sigma, \mu, \mu_H, D)$  at 77K

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 $N (10^{18} \text{ cm}^{-3})$

3	0.68, 1.883, 3.685, 2.60	0.54, 1.613, 3.325, 2.07	0.53, 1.600, 3.308, 2.04	0.52, 1.586, 3.290, 2.02
10	2.61, 1.758, 2.080, 6.40	2.28, 1.569, 1.863, 5.65	2.27, 1.560, 1.853, 5.61	2.25, 1.551, 1.843, 5.57
40	9.40, 1.495, 1.538, 14.0	8.30, 1.325, 1.364, 12.4	8.25, 1.317, 1.356, 12.3	8.20, 1.309, 1.347, 12.2
70	15.9, 1.433, 1.453, 19.6	14.0, 1.269, 1.286, 17.3	13.9, 1.261, 1.278, 17.2	13.8, 1.253, 1.270, 17.1

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**Table 4n.** In the lightly degenerate n-type  $\text{InSb}_{1-x}\text{As}_x$  alloy, in which  $N=5 \times 10^{17} \text{ cm}^{-3}$ , and for  $T=3\text{K}$  and  $80\text{K}$ , the numerical results of various thermoelectric coefficients are reported. Further, their variations with increasing  $r_{d(a)}$  are represented by the arrows: ↗ (increase), and ↘ (decrease).

Donor		P	As	Sb	Sn
<b>For x=0,</b>					
$\xi_{n(T=3K)}$	↘	87.31	86.776	86.209	86.178
$\xi_{n(T=80K)}$	↘	3.30	3.270	3.240	3.238
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{\text{cm} \times K} \right)$	↘	3.076	2.678	2.383	2.369
$\kappa_{(T=80K)} \left( \frac{10^{-4} \times W}{\text{cm} \times K} \right)$	↘	8.330	7.213	6.380	6.340
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.491	6.531	6.574	6.576
$-S_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	13.201	13.260	13.324	13.327
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↗	4.322	4.349	4.377	4.379
$VC_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	6.477	6.472	6.463	6.4629
$-TS_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.484	6.523	6.566	6.568
$-TS_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↗	9.715	9.708	9.695	9.694
$-Pt_{(T=3K)}(10^{-5} \times V)$	↘	1.947	1.959	1.972	1.973
$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	1.056	1.061	1.066	1.0662
$ZT_{(T=3K)} (10^{-3})$	↗	1.725	1.746	1.769	1.770
$ZT_{(T=80K)}$	↗	0.713	0.7197	0.72665	0.72704
<b>For x=0.5,</b>					
$\xi_{n(T=3K)}$	↘	91.81	91.219	90.590	90.555
$\xi_{n(T=80K)}$	↘	3.53	3.497	3.466	3.464
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{\text{cm} \times K} \right)$	↘	3.209	2.797	2.492	2.478
$\kappa_{(T=80K)} \left( \frac{10^{-4} \times W}{\text{cm} \times K} \right)$	↘	9.054	7.855	6.960	6.918
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.173	6.213	6.256	6.259
$-S_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	12.714	12.776	12.843	12.846
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↗	4.111	4.138	4.166	4.168
$VC_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↗	6.402	6.422	6.440	6.4408
$-TS_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.167	6.206	6.249	6.252
$-TS_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	9.603	9.633	9.660	9.661
$-Pt_{(T=3K)}(10^{-5} \times V)$	↘	1.852	1.864	1.877	1.878
$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	1.017	1.022	1.0274	1.0277

$ZT_{(T=3K)} (10^{-3})$	↗	1.560	1.580	1.602	1.603
$ZT_{(T=80K)}$	↗	0.662	0.668	0.6751	0.6755
<b>For x=1,</b>					
$\xi_{n(T=3K)}$	↘	96.79	96.131	95.424	95.384
$\xi_{n(T=80K)}$	↘	3.77	3.738	3.704	3.702
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{cm \times K} \right)$	↘	3.382	2.951	2.632	2.617
$\kappa_{(T=80K)} \left( \frac{10^{-4} \times W}{cm \times K} \right)$	↘	9.869	8.580	7.619	7.574
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	5.856	5.896	5.940	5.942
$-S_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	12.214	12.278	12.347	12.351
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↗	3.900	3.927	3.956	3.957
$VC_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↗	6.161	6.224	6.244	6.246
$-TS_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	5.850	5.890	5.934	5.936
$-TS_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	9.241	9.298	9.356	9.359
$-Pt_{(T=3K)} (10^{-5} \times V)$	↘	1.757	1.769	1.7819	1.7826
$-Pt_{(T=80K)} (10^{-2} \times V)$	↘	0.977	0.982	0.9878	0.9881
$ZT_{(T=3K)} (10^{-3})$	↗	1.403	1.423	1.444	1.445
$ZT_{(T=80K)}$	↗	0.611	0.617	0.6240	0.6244

**Table 4p.** In the lightly degenerate p-type  $InSb_{1-x}As_x$  alloy, in which  $N=5 \times 10^{18} \text{ cm}^{-3}$ , and for T=3K and 80K, the numerical results of various thermoelectric coefficients are reported. Further, their variations with increasing  $r_{d(a)}$  are represented by the arrows: ↗ (increase), and ↘ (decrease).

Acceptor		Ga	Mg	In	Cd
<b>For x=0,</b>					
$\xi_{p(T=3K)}$	↘	86.689	82.794	82.571	82.341
$\xi_{p(T=80K)}$	↘	3.265	3.060	3.048	3.035
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{cm \times K} \right)$	↘	6.649	5.583	5.531	5.478
$\kappa_{(T=80K)} \left( \frac{10^{-3} \times W}{cm \times K} \right)$	↘	1.789	1.436	1.419	1.401
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.538	6.845	6.863	6.882
$-S_{(T=80K)} \left( \frac{10^{-4} \times V}{K} \right)$	↘	1.327	1.371	1.374	1.376
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↗	4.353	4.557	4.569	4.582
$VC_{(T=80K)} \left( \frac{10^{-5} \times V}{K} \right)$	↘	6.471	6.321	6.306	6.290
$-TS_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right)$	↘	6.530	6.836	6.854	6.873

$-Ts_{(T=30K)} \left( \frac{10^{-5} \times V}{K} \right) \nearrow$	9.707	9.482	9.459	9.435
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.961	2.053	2.059	2.065
$-Pt_{(T=30K)}(10^{-2} \times V) \searrow$	1.061	1.097	1.099	1.101
$ZT_{(T=3K)}(10^{-3}) \nearrow$	1.749	1.918	1.928	1.939
$ZT_{(T=30K)} \nearrow$	0.721	0.7696	0.772	0.775

**For x=0.5,**

$\xi_p(T=3K) \searrow$	102.48	98.88	98.67	98.46
$\xi_p(T=30K) \searrow$	4.029	3.866	3.857	3.847
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{cm \times K} \right) \searrow$	7.635	6.498	6.443	6.387
$\kappa_{(T=30K)} \left( \frac{10^{-3} \times W}{cm \times K} \right) \searrow$	2.285	1.917	1.899	1.880
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \searrow$	5.531	5.732	5.744	5.757
$-S_{(T=30K)} \left( \frac{10^{-4} \times V}{K} \right) \searrow$	1.170	1.202	1.204	1.206
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \nearrow$	3.684	3.818	3.826	3.834
$VC_{(T=30K)} \left( \frac{10^{-5} \times V}{K} \right) \nearrow$	5.815	6.037	6.049	6.062
$-Ts_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \searrow$	5.526	5.727	5.739	5.751
$-Ts_{(T=30K)} \left( \frac{10^{-5} \times V}{K} \right) \searrow$	8.723	9.055	9.074	9.093
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.659	1.720	1.723	1.727
$-Pt_{(T=30K)}(10^{-2} \times V) \searrow$	0.936	0.961	0.963	0.965
$ZT_{(T=3K)}(10^{-3}) \nearrow$	1.252	1.345	1.351	1.356
$ZT_{(T=30K)} \nearrow$	0.560	0.591	0.593	0.595

**For x=1,**

$\xi_p(T=3K) \searrow$	123.47	120.22	120.03	119.84
$\xi_p(T=30K) \searrow$	4.875	4.752	4.745	4.737
$\kappa_{(T=3K)} \left( \frac{10^{-5} \times W}{cm \times K} \right) \searrow$	8.950	7.711	7.651	7.590
$\kappa_{(T=30K)} \left( \frac{10^{-3} \times W}{cm \times K} \right) \searrow$	2.728	2.354	2.336	2.317
$-S_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \searrow$	4.591	4.715	4.722	4.730
$-S_{(T=30K)} \left( \frac{10^{-4} \times V}{K} \right) \searrow$	1.022	1.041	1.043	1.044
$VC_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \nearrow$	3.059	3.141	3.146	3.151
$VC_{(T=30K)} \left( \frac{10^{-5} \times V}{K} \right) \nearrow$	4.923	5.001	5.014	5.020
$-Ts_{(T=3K)} \left( \frac{10^{-6} \times V}{K} \right) \searrow$	4.588	4.712	4.719	4.727
$-Ts_{(T=30K)} \left( \frac{10^{-5} \times V}{K} \right) \searrow$	7.384	7.513	7.521	7.530
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.377	1.414	1.417	1.419

$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	0.817	0.833	0.834	0.835
$ZT_{(T=8K)}(10^{-3})$	↗	0.863	0.910	0.913	0.916
$ZT_{(T=80K)}$	↗	0.427	0.444	0.445	0.446

**Table 5n:** Here, for a given  $N$  and with increasing  $T$ , the reduced Fermi-energy  $\xi_n$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing  $T$ : (i) for  $\xi_n \approx 1.8138$ , while the numerical results of  $S$  present a same minimum  $(S)_{min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$ , those of  $ZT$  show a same maximum  $(ZT)_{max.} = 1$ , (ii) for  $\xi_n = 1$ , those of  $S$ ,  $ZT$ ,  $(ZT)_{Mott}$ ,  $VC$ , and  $T_s$  present the same results:  $-1.322 \times 10^{-4} \frac{V}{K}$ , 0.715, 3.290,  $-1.105 \times 10^{-4} \frac{V}{K}$ , and  $1.657 \times 10^{-4} \frac{V}{K}$ , respectively, and (iii) for  $\xi_n \approx 1.8138$ ,  $(ZT)_{Mott} = 1$ .

For  $x=0$ ,

In the degenerate P-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_P)$ , one gets:

T(K)	↗	10	<b>10.528</b>	12	<b>14.325731</b>	14.5
$\xi_n$	↘	1.974	<b>1.8138</b>	1.442	<b>1</b>	0.972
$S(10^{-4} \frac{V}{K})$		-1.557	↘ <b>-1.563</b> ↗	-1.523	↗ <b>-1.322</b> ↗	-1.301
ZT		0.993	↗ <b>1</b> ↘	0.949	↘ <b>0.715</b> ↘	0.693
$(ZT)_{Mott}$	↗	0.844	<b>1</b>	1.581	<b>3.290</b>	3.484
$VC(10^{-4} \frac{V}{K})$		0.142	↘ $-7.52 \times 10^{-5}$ ↘	-0.423	↘ <b>-1.105</b> ↘	-1.153
$T_s(10^{-4} \frac{V}{K})$		-0.213	↗ $1.13 \times 10^{-4}$ ↗	0.635	↗ <b>1.657</b> ↗	1.730
$Pt(10^{-3}V)$		-1.557	↘ -1.645 ↘	-1.827	↘ -1.893 ↗	-1.887

In the degenerate As-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{As})$ , one gets:

T(K)	↗	10	<b>12.813</b>	15	<b>17.435302</b>	17.5
$\xi_n$	↘	2.685	<b>1.8138</b>	1.372	<b>1</b>	0.991
$S(10^{-4} \frac{V}{K})$		-1.450	↘ <b>-1.563</b> ↗	-1.504	↗ <b>-1.322</b> ↗	-1.315
ZT		0.860	↗ <b>1</b> ↘	0.926	↘ <b>0.715</b> ↘	0.708
$(ZT)_{Mott}$	↗	0.456	<b>1</b>	1.748	<b>3.290</b>	3.348
$VC(10^{-4} \frac{V}{K})$		0.547	↘ $-2.35 \times 10^{-5}$ ↘	-0.519	↘ <b>-1.105</b> ↘	-1.120
$T_s(10^{-4} \frac{V}{K})$		-0.820	↗ $3.53 \times 10^{-5}$ ↗	0.779	↗ <b>1.657</b> ↗	1.680
$Pt(10^{-3}V)$		-1.450	↘ -2.003 ↘	-2.256	↘ -2.304 ↗	-2.302

In the degenerate Sb-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{Sb})$ , one gets:

T(K)	↗	10	<b>15.0335</b>	16	<b>20.4571662</b>	20.5
$\xi_n$	↘	3.382	<b>1.8138</b>	1.631	<b>1</b>	0.995
$S(10^{-4} \frac{V}{K})$		-1.302	↘ <b>-1.563</b> ↗	-1.554	↗ <b>-1.322</b> ↗	-1.318
ZT		0.694	↗ <b>1</b> ↘	0.989	↘ <b>0.715</b> ↘	0.711
$(ZT)_{Mott}$	↗	0.287	<b>1</b>	1.236	<b>3.290</b>	3.322

$VC \left(10^{-4} \frac{V}{K}\right)$	0.647 ↘	$0.21 \times 10^{-5}$ ↘	-0.191 ↘	<b>-1.105</b> ↘	-1.113
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.971 ↗	$-3.22 \times 10^{-5}$ ↗	0.286 ↗	<b>1.657</b> ↗	1.670
$Pt (10^{-3}V)$	-1.302 ↘	-2.350 ↘	-2.487 ↘	-2.704 ↗	-2.702

In the degenerate Sn-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{Sn})$ , one gets:

T(K)	↗	10	<b>15.1525</b>	16	<b>20.6188</b>	20.7
$\xi_n$	↘	3.418	<b>1.8138</b>	1.654	<b>1</b>	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.294 ↘	<b>-1.563</b> ↗	-1.556 ↗	<b>-1.322</b> ↗	-1.315	
ZT	0.686 ↗	<b>1</b> ↘	0.991 ↘	<b>0.715</b> ↘	0.708	
$(ZT)_{Mott}$	↗	0.281	<b>1</b>	1.203	<b>3.290</b>	3.351
$VC \left(10^{-4} \frac{V}{K}\right)$	0.646 ↘	$-0.20 \times 10^{-5}$ ↘	-0.165 ↘	<b>-1.105</b> ↘	-1.121	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.969 ↗	$3.08 \times 10^{-5}$ ↗	0.248 ↗	<b>1.657</b> ↗	1.681	
$Pt (10^{-3}V)$	-1.294 ↘	-2.368 ↘	-2.490 ↘	-2.725 ↗	-2.722	

For x=0.5,

In the degenerate P-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_p)$ , one gets:

T(K)	↗	10	<b>11.4883</b>	12	<b>15.6330543</b>	15.7
$\xi_n$	↘	2.269	<b>1.8138</b>	1.685	<b>1</b>	0.990
$S \left(10^{-4} \frac{V}{K}\right)$	-1.524 ↘	<b>-1.563</b> ↗	-1.559 ↗	<b>-1.322</b> ↗	-1.314	
ZT	0.951 ↗	<b>1</b> ↘	0.994 ↘	<b>0.715</b> ↘	0.707	
$(ZT)_{Mott}$	↗	0.639	<b>1</b>	1.159	<b>3.290</b>	3.357
$VC \left(10^{-4} \frac{V}{K}\right)$	0.352 ↘	$3.95 \times 10^{-5}$ ↘	-0.131 ↘	<b>-1.105</b> ↘	-1.122	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.528 ↗	$-5.92 \times 10^{-5}$ ↗	0.197 ↗	<b>1.657</b> ↗	1.683	
$Pt (10^{-3}V)$	-1.524 ↘	-1.796 ↘	-1.870 ↘	-2.066 ↗	-2.064	

In the degenerate As-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{As})$ , one gets:

T(K)	↗	10	<b>13.9822</b>	15	<b>19.0263965</b>	19.1
$\xi_n$	↘	3.056	<b>1.8138</b>	1.610	<b>1</b>	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.372 ↘	<b>-1.563</b> ↗	-1.552 ↗	<b>-1.322</b> ↗	-1.315	
ZT	0.770 ↗	<b>1</b> ↘	0.986 ↘	<b>0.715</b> ↘	0.708	
$(ZT)_{Mott}$	↗	0.352	<b>1</b>	1.271	<b>3.290</b>	3.350
$VC \left(10^{-4} \frac{V}{K}\right)$	0.632 ↘	$-7.62 \times 10^{-6}$ ↘	-0.216 ↘	<b>-1.105</b> ↘	-1.120	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.948 ↗	$1.14 \times 10^{-5}$ ↗	0.325 ↗	<b>1.657</b> ↗	1.681	
$Pt (10^{-3}V)$	-1.372 ↘	-2.185 ↘	-2.328 ↘	-2.515 ↗	-2.512	

In the degenerate Sb-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{Sb})$ , one gets:

T(K)	↗	10	<b>16.4055</b>	17	<b>22.324027</b>	22.4
$\xi_n$	↘	3.782	<b>1.8138</b>	1.708	<b>1</b>	0.992

$S \left(10^{-4} \frac{V}{K}\right)$	-1.219 ↘	<b>-1.563</b> ↗	-1.560 ↗	<b>-1.322</b> ↗	-1.316
ZT	0.608 ↗	<b>1</b> ↘	0.996 ↘	<b>0.715</b> ↘	0.709
$(ZT)_{Mott}$ ↗	0.230	<b>1</b>	1.128	<b>3.290</b>	3.343
$VC \left(10^{-4} \frac{V}{K}\right)$	0.614 ↘	<b><math>6.02 \times 10^{-6}</math></b> ↘	-0.106 ↘	<b>-1.105</b> ↘	-1.118
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.922 ↗	<b><math>-9.03 \times 10^{-6}</math></b> ↗	0.160 ↗	<b>1.657</b> ↗	1.678
Pt ( $10^{-3}V$ )	-1.219 ↘	-2.564 ↘	-2.652 ↘	-2.950 ↗	-2.948

In the degenerate Sn-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{Sn})$ , one gets:

T(K)	↗	10	<b>16.535</b>	17	<b>22.500411</b>	22.6
$\xi_n$	↘	3.818	<b>1.8138</b>	1.731	<b>1</b>	0.990
$S \left(10^{-4} \frac{V}{K}\right)$	-1.212 ↘	<b>-1.563</b> ↗	-1.561 ↗	<b>-1.322</b> ↗	-1.314	
ZT	0.601 ↗	<b>1</b> ↘	0.998 ↘	<b>0.715</b> ↘	0.707	
$(ZT)_{Mott}$ ↗	0.226	<b>1</b>	1.098	<b>3.290</b>	3.359	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.610 ↘	<b><math>2.73 \times 10^{-5}</math></b> ↘	-0.082 ↘	<b>-1.105</b> ↘	-1.123	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.915 ↗	<b><math>-4.09 \times 10^{-5}</math></b> ↗	0.124 ↗	<b>1.657</b> ↗	1.684	
Pt ( $10^{-3}V$ )	-1.212 ↘	-2.584 ↘	-2.654 ↘	-2.974 ↗	-2.970	

For x=1,

In the degenerate P-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_P)$ , one gets:

T(K)	↗	10	<b>12.633</b>	12.7	<b>17.18905</b>	17.2
$\xi_n$	↘	2.628	<b>1.8138</b>	1.797	<b>1</b>	0.998
$S \left(10^{-4} \frac{V}{K}\right)$	-1.461 ↘	<b>-1.563</b> ↗	-1.563 ↗	<b>-1.322</b> ↗	-1.321	
ZT	0.874 ↗	<b>1</b> ↘	0.999 ↘	<b>0.715</b> ↘	0.714	
$(ZT)_{Mott}$ ↗	0.476	<b>1</b>	1.018	<b>3.290</b>	3.300	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.526 ↘	<b><math>-2.46 \times 10^{-4}</math></b> ↘	-0.016 ↘	<b>-1.105</b> ↘	-1.107	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.789 ↗	<b><math>3.69 \times 10^{-4}</math></b> ↗	0.023 ↗	<b>1.657</b> ↗	1.661	
Pt ( $10^{-3}V$ )	-1.461 ↘	-1.974 ↘	-1.985 ↘	-2.272 ↗	-2.271	

In the degenerate As-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDn}(r_{As})$ , one gets:

T(K)	↗	10	<b>15.375</b>	16	<b>20.920139</b>	21
$\xi_n$	↘	3.484	<b>1.8138</b>	1.695	<b>1</b>	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.280 ↘	<b>-1.563</b> ↗	-1.559 ↗	<b>-1.322</b> ↗	-1.315	
ZT	0.671 ↗	<b>1</b> ↘	0.995 ↘	<b>0.715</b> ↘	0.708	
$(ZT)_{Mott}$ ↗	0.271	<b>1</b>	1.144	<b>3.290</b>	3.349	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.643 ↘	<b><math>-2.19 \times 10^{-4}</math></b> ↘	-0.120 ↘	<b>-1.105</b> ↘	-1.120	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.964 ↗	<b><math>3.3 \times 10^{-4}</math></b> ↗	0.180 ↗	<b>1.657</b> ↗	1.680	
Pt ( $10^{-3}V$ )	-1.280 ↘	-2.403 ↘	-2.495 ↘	-2.765 ↗	-2.762	



In the degenerate Sb-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $N = 2 \times N_{\text{CDn}}(r_{\text{Sb}})$ , one gets:

T(K)	↗	10	<b>18.04</b>	18.5	<b>24.54599</b>	24.6
$\xi_n$	↘	4.212	<b>1.8138</b>	1.738	<b>1</b>	0.995
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.135	<b>-1.563</b>	↗ -1.561	↗ <b>-1.322</b>	↗ -1.318
ZT		0.528	<b>1</b>	↘ 0.998	↘ <b>0.715</b>	↘ 0.711
$(ZT)_{\text{Mott}}$	↗	0.185	<b>1</b>	1.089	<b>3.290</b>	3.324
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.557	<b><math>-2.55 \times 10^{-4}</math></b>	↘ -0.075	↘ <b>-1.105</b>	↘ -1.114
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.835	<b><math>3.82 \times 10^{-4}</math></b>	↗ 0.112	↗ <b>1.657</b>	↗ 1.671
Pt ( $10^{-3}\text{V}$ )		-1.135	<b>-2.820</b>	↘ -2.889	↘ <b>-3.244</b>	↘ -3.242

In the degenerate Sn-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $N = 2 \times N_{\text{CDn}}(r_{\text{Sn}})$ , one gets:

T(K)	↗	10	<b>18.1809</b>	19	<b>24.73993</b>	24.8
$\xi_n$	↘	4.248	<b>1.8138</b>	1.683	<b>1</b>	0.994
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.129	<b>-1.563</b>	↗ -1.559	↗ <b>-1.322</b>	↗ -1.318
ZT		0.522	<b>1</b>	↘ 0.994	↘ <b>0.715</b>	↘ 0.711
$(ZT)_{\text{Mott}}$	↗	0.182	<b>1</b>	1.161	<b>3.290</b>	3.328
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.552	<b><math>6.15 \times 10^{-6}</math></b>	↘ -0.133	↘ <b>-1.105</b>	↘ -1.115
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.828	<b><math>-9.23 \times 10^{-6}</math></b>	↗ 0.199	↗ <b>1.657</b>	↗ 1.672
Pt ( $10^{-3}\text{V}$ )		-1.129	<b>-2.842</b>	↘ -2.961	↘ <b>-3.270</b>	↘ -3.268

**Table 5p:** Here, for a given  $N$  and with increasing  $T$ , the reduced Fermi-energy  $\xi_p$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing  $T$ : (i) for  $\xi_p \approx 1.8138$ , while the numerical results of  $S$  present a same minimum  $(S)_{\text{min.}} (\approx -1.563 \times 10^{-4} \frac{\text{V}}{\text{K}})$ , those of  $ZT$  show a same maximum  $(ZT)_{\text{max.}} = 1$ , (ii) for  $\xi_p = 1$ , those of  $S$ ,  $ZT$ ,  $(ZT)_{\text{Mott}}$ ,  $VC$ , and  $T_s$  present the same results:  $-1.322 \times 10^{-4} \frac{\text{V}}{\text{K}}$ ,  $0.715$ ,  $3.290$ ,  $-1.105 \times 10^{-4} \frac{\text{V}}{\text{K}}$ , and  $1.657 \times 10^{-4} \frac{\text{V}}{\text{K}}$ , respectively, and (iii) for  $\xi_p \approx 1.8138$ ,  $(ZT)_{\text{Mott}} = 1$ .

For  $x=0$ ,

In the degenerate Ga-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $N = 2 \times N_{\text{CDp}}(r_{\text{Ga}})$ , one gets:

T(K)	↗	30	<b>52.184</b>	55	<b>71.008677</b>	71.5
$\xi_p$	↘	4.048	<b>1.8138</b>	1.659	<b>1</b>	0.984
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.166	<b>-1.563</b>	↗ -1.557	↗ <b>-1.322</b>	↗ -1.310
ZT		0.557	<b>1</b>	↘ 0.992	↘ <b>0.715</b>	↘ 0.703
$(ZT)_{\text{Mott}}$	↗	0.201	<b>1</b>	1.195	<b>3.290</b>	3.399
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.579	<b><math>-5.42 \times 10^{-5}</math></b>	↘ -0.160	↘ <b>-1.105</b>	↘ -1.132
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.868	<b><math>8.13 \times 10^{-5}</math></b>	↗ 0.239	↗ <b>1.657</b>	↗ 1.699

Pt ( $10^{-2}V$ )    -3.499   ↘    -8.156   ↘    -8.562   ↘    -9.385   ↗    -9.367

In the degenerate Mg-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(\Gamma_{Mg})$ , one gets:

T(K)	↗	30	<b>59.722</b>	70	<b>81.26823</b>	81.3
$\xi_p$	↘	4.658	<b>1.8138</b>	1.369	<b>1</b>	0.999
$S \left(10^{-4} \frac{V}{K}\right)$		-1.057	↘ <b>-1.563</b> ↗	-1.503	↗ <b>-1.322</b> ↗	-1.321
ZT		0.457	↗ <b>1</b> ↘	0.925	↘ <b>0.715</b> ↘	0.714
$(ZT)_{Mott}$	↗	0.152	<b>1</b>	1.756	<b>3.290</b>	3.296
$VC \left(10^{-4} \frac{V}{K}\right)$		<b>0.508</b>	↘ $2.86 \times 10^{-5}$ ↘	-0.524	↘ <b>-1.105</b> ↘	-1.106
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.762	↗ $-4.30 \times 10^{-5}$ ↗	0.786	↗ <b>1.657</b> ↗	1.660
Pt ( $10^{-2}V$ )		-0.317	↘ -0.934 ↘	-1.052	↘ -1.07412 ↗	-1.07402

In the degenerate In-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(\Gamma_{In})$ , one gets:

T(K)	↗	30	<b>60.135</b>	70	<b>81.828665</b>	81.9
$\xi_p$	↘	4.689	<b>1.8138</b>	1.387	<b>1</b>	0.998
$S \left(10^{-4} \frac{V}{K}\right)$		-1.052	↘ <b>-1.563</b> ↗	-1.508	↗ <b>-1.322</b> ↗	-1.320
ZT		0.453	↗ <b>1</b> ↘	0.931	↘ <b>0.715</b> ↘	0.713
$(ZT)_{Mott}$	↗	0.150	<b>1</b>	1.710	<b>3.290</b>	3.303
$VC \left(10^{-4} \frac{V}{K}\right)$		<b>0.506</b>	↘ $-2.68 \times 10^{-5}$ ↘	-0.499	↘ <b>-1.105</b> ↘	-1.108
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.759	↗ $4.02 \times 10^{-5}$ ↗	0.748	↗ <b>1.657</b> ↗	1.663
Pt ( $10^{-2}V$ )		-0.315	↘ -0.940 ↘	-1.056	↘ -1.08153 ↗	-1.08129

In the degenerate Cd-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(\Gamma_{Cd})$ , one gets:

T(K)	↗	30	<b>60.558</b>	70	<b>82.404885</b>	82.5
$\xi_p$	↘	4.721	<b>1.8138</b>	1.405	<b>1</b>	0.997
$S \left(10^{-4} \frac{V}{K}\right)$		-1.046	↘ <b>-1.563</b> ↗	-1.513	↗ <b>-1.322</b> ↗	-1.320
ZT		0.448	↗ <b>1</b> ↘	0.938	↘ <b>0.715</b> ↘	0.713
$(ZT)_{Mott}$	↗	0.147	<b>1</b>	1.666	<b>3.290</b>	3.308
$VC \left(10^{-4} \frac{V}{K}\right)$		<b>0.503</b>	↘ $-4.87 \times 10^{-6}$ ↘	-0.473	↘ <b>-1.105</b> ↘	-1.109
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.755	↗ $7.30 \times 10^{-6}$ ↗	0.710	↗ <b>1.657</b> ↗	1.664
Pt ( $10^{-2}V$ )		-0.314	↘ -0.9465 ↘	-1.059	↘ -1.08915 ↗	-1.0888

For  $x=0.5$ ,

In the degenerate Ga-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(\Gamma_{Ga})$ , one gets:

T(K)	↗	30	<b>52.449</b>	55	<b>71.37119</b>	71.5
$\xi_p$	↘	4.071	<b>1.8138</b>	1.674	<b>1</b>	0.996
$S \left(10^{-4} \frac{V}{K}\right)$		-1.162	↘ <b>-1.563</b> ↗	-1.558	↗ <b>-1.322</b> ↗	-1.319
ZT		0.553	↗ <b>1</b> ↘	0.993	↘ <b>0.715</b> ↘	0.712

$(ZT)_{Mott}$	↗	0.198	1	1.174	3.290	3.318
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.576	$2.37 \times 10^{-5}$	-0.143	-1.105	-1.112
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.863	$-3.55 \times 10^{-5}$	0.215	1.657	1.668
Pt ( $10^{-2}V$ )	↘	-0.349	-0.820	-0.857	-0.9433	-0.9429

In the degenerate Mg-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{Mg})$ , one gets:

T(K)	↗	30	60.028	70	81.68312	82
$\xi_p$	↘	4.681	1.8138	1.382	1	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.053	-1.563	-1.507	-1.322	-1.315
ZT	↗	0.454	1	0.930	0.715	0.708
$(ZT)_{Mott}$	↗	0.150	1	1.722	3.290	3.350
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.506	$-2.49 \times 10^{-5}$	-0.505	-1.105	-1.120
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.760	$3.73 \times 10^{-5}$	0.758	1.657	1.681
Pt ( $10^{-2}V$ )	↘	-0.316	-0.938	-1.0549	-1.07961	-1.07850

In the degenerate In-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{In})$ , one gets:

T(K)	↗	30	60.442	70	82.246416	82.5
$\xi_p$	↘	4.712	1.8138	1.400	1	0.993
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.048	-1.563	-1.512	-1.322	-1.316
ZT	↗	0.449	1	0.936	0.715	0.709
$(ZT)_{Mott}$	↗	0.148	1	1.678	3.290	3.338
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.504	$-2.67 \times 10^{-5}$	-0.480	-1.105	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.756	$4.01 \times 10^{-5}$	0.720	1.657	1.676
Pt ( $10^{-2}V$ )	↘	-0.314	-0.945	-1.058	-1.08705	-1.0862

In the degenerate Cd-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{Cd})$ , one gets:

T(K)	↗	30	60.8672	70	82.825577	83
$\xi_p$	↘	4.745	1.8138	1.419	1	0.995
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.043	-1.563	-1.517	-1.322	-1.318
ZT	↗	0.450	1	0.942	0.715	0.711
$(ZT)_{Mott}$	↗	0.146	1	1.6634	3.290	3.323
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.501	$-6.78 \times 10^{-6}$	-0.455	-1.105	-1.114
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.752	$1.02 \times 10^{-5}$	0.682	1.657	1.670
Pt ( $10^{-2}V$ )	↘	-0.313	-0.951	-1.062	-1.09471	-1.09411

For x=1,

In the degenerate Ga-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{Ga})$ , one gets:

T(K)	↗	30	52.177	55	71.00113	71.5
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$\xi_p$	↘	4.047	<b>1.8138</b>	1.659	<b>1</b>	0.983
$S \left(10^{-4} \frac{V}{K}\right)$		-1.166	↘ <b>-1.563</b> ↗	-1.557	↗ <b>-1.322</b> ↗	-1.310
ZT		0.557	↗ <b>1</b> ↘	0.992	↘ <b>0.715</b> ↘	0.702
$(ZT)_{Mott}$	↗	0.201	<b>1</b>	1.196	<b>3.290</b>	3.400
$VC \left(10^{-4} \frac{V}{K}\right)$		0.579	↘ $2.66 \times 10^{-5}$ ↘	-0.160	↘ <b>-1.105</b> ↘	-1.133
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.868	↗ $-3.99 \times 10^{-5}$ ↗	0.240	↗ <b>1.657</b> ↗	1.699
Pt ( $10^{-2}V$ )		-0.350	↘ -0.815 ↘	-0.856	↘ -0.938 ↗	-0.937

In the degenerate Mg-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{Mg})$ , one gets:

T(K)	↗	30	<b>59.716</b>	70	<b>81.259592</b>	81.5
$\xi_p$	↘	4.657	<b>1.8138</b>	1.368	<b>1</b>	0.993
$S \left(10^{-4} \frac{V}{K}\right)$		-1.057	↘ <b>-1.563</b> ↗	-1.503	↗ <b>-1.322</b> ↗	-1.317
ZT		0.457	↗ <b>1</b> ↘	0.925	↘ <b>0.715</b> ↘	0.710
$(ZT)_{Mott}$	↗	0.152	<b>1.0009</b>	1.756	<b>3.290</b>	3.336
$VC \left(10^{-4} \frac{V}{K}\right)$		0.508	↘ $1.17 \times 10^{-5}$ ↘	-0.524	↘ <b>-1.105</b> ↘	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.763	↗ $-1.76 \times 10^{-5}$ ↗	0.786	↗ <b>1.657</b> ↗	1.675
Pt ( $10^{-2}V$ )		-0.317	↘ -0.933 ↘	-1.052	↘ -1.07401 ↗	-1.0732

In the degenerate In-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{In})$ , one gets:

T(K)	↗	30	<b>60.128</b>	70	<b>81.819968</b>	82
$\xi_p$	↘	4.689	<b>1.8138</b>	1.386	<b>1</b>	0.995
$S \left(10^{-4} \frac{V}{K}\right)$		-1.052	↘ <b>-1.563</b> ↗	-1.508	↗ <b>-1.322</b> ↗	-1.318
ZT		0.453	↗ <b>1</b> ↘	0.931	↘ <b>0.715</b> ↘	0.711
$(ZT)_{Mott}$	↗	0.150	<b>1</b>	1.711	<b>3.290</b>	3.324
$VC \left(10^{-4} \frac{V}{K}\right)$		0.506	↘ $2.54 \times 10^{-6}$ ↘	-0.499	↘ <b>-1.105</b> ↘	-1.114
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.759	↗ $-3.81 \times 10^{-6}$ ↗	0.748	↗ <b>1.657</b> ↗	1.671
Pt ( $10^{-2}V$ )		-0.315	↘ -0.940 ↘	-1.056	↘ -1.081417 ↗	-1.0808

In the degenerate Cd-  $InSb_{1-x}As_x$  alloy, for  $N = 2 \times N_{CDP}(r_{Cd})$ , one gets:

T(K)	↗	30	<b>60.552</b>	70	<b>82.396125</b>	82.5
$\xi_p$	↘	4.721	<b>1.8138</b>	1.405	<b>1</b>	0.997
$S \left(10^{-4} \frac{V}{K}\right)$		-1.046	↘ <b>-1.563</b> ↗	-1.513	↗ <b>-1.322</b> ↗	-1.320
ZT		0.448	↗ <b>1</b> ↘	0.937	↘ <b>0.715</b> ↘	0.713
$(ZT)_{Mott}$	↗	0.148	<b>1</b>	1.666	<b>3.290</b>	3.309
$VC \left(10^{-4} \frac{V}{K}\right)$		0.503	↘ $-2.58 \times 10^{-5}$ ↘	-0.473	↘ <b>-1.105</b> ↘	-1.110
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.755	↗ $3.87 \times 10^{-5}$ ↗	0.710	↗ <b>1.657</b> ↗	1.665
Pt ( $10^{-2}V$ )		-0.314	↘ -0.946 ↘	-1.059	↘ -1.08903 ↗	-1.0887

**Table 6n.** Here, for a given T and with decreasing N, the reduced Fermi-energy  $\xi_n$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T: (i) for  $\xi_n \approx 1.8138$ , while the numerical results of S present a same minimum  $(S)_{\min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$ , those of ZT show a same maximum  $(ZT)_{\max} = 1$ , (ii) for  $\xi_n = 1$ , those of S, ZT,  $(ZT)_{\text{Mott}}$ , VC, and  $T_s$  present the same results:  $-1.322 \times 10^{-4} \frac{V}{K}$ , 0.715, 3.290,  $-1.105 \times 10^{-4} \frac{V}{K}$ , and  $1.657 \times 10^{-4} \frac{V}{K}$ , respectively, and (iii) for  $\xi_n \approx 1.8138$ ,  $(ZT)_{\text{Mott}} = 1$ .

For x=0,

In the degenerate P-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T= 10.528 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	3	<b>2.5942062</b>	2.3	<b>2.11428385</b>	2.11
$\xi_n$	↘	2.42542	<b>1.8138</b>	1.336	<b>1</b>	0.992
$S(10^{-4} \frac{V}{K})$		-1.499	↘ <b>-1.563</b> ↗	-1.493	↗ <b>-1.322</b> ↗	-1.316
ZT		0.920	↗ <b>1</b> ↘	0.912	↘ <b>0.715</b> ↘	0.709
$(ZT)_{\text{Mott}}$	↗	0.559	<b>1</b>	1.844	<b>3.290</b>	3.345
$VC(10^{-4} \frac{V}{K})$		0.438	↘ $-7.52 \times 10^{-5}$ ↘	-0.571	↘ <b>-1.105</b> ↘	-1.119
$T_s(10^{-4} \frac{V}{K})$		-0.657	↗ $1.13 \times 10^{-4}$ ↗	0.856	↗ <b>1.657</b> ↗	1.678
Pt ( $10^{-3}V$ )		-1.578	↘ -1.645 ↗	-1.571	↗ -1.391 ↗	-1.385

In the degenerate As-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T= 12.813 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4	<b>3.4831608</b>	3	<b>2.8387545</b>	2.838
$\xi_n$	↘	2.395	<b>1.8138</b>	1.221	<b>1</b>	0.999
$S(10^{-4} \frac{V}{K})$		-1.504	↘ <b>-1.563</b> ↗	-1.448	↗ <b>-1.322</b> ↗	-1.3209
ZT		0.927	↗ <b>1</b> ↘	0.858	↘ <b>0.715</b> ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.574	<b>1</b>	2.206	<b>3.290</b>	3.297
$VC(10^{-4} \frac{V}{K})$		0.422	↘ $-2.35 \times 10^{-5}$ ↘	-0.742	↘ <b>-1.105</b> ↘	-1.107
$T_s(10^{-4} \frac{V}{K})$		-0.633	↗ $3.53 \times 10^{-5}$ ↗	1.114	↗ <b>1.657</b> ↗	1.660
Pt ( $10^{-3}V$ )		-1.928	↘ -2.003 ↗	-1.856	↗ -1.693 ↗	-1.692

In the degenerate Sb-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T= 15.0335 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4.5	<b>4.4268778</b>	4	<b>3.6078456</b>	3.607
$\xi_n$	↘	1.880	<b>1.8138</b>	1.411	<b>1</b>	0.999
$S(10^{-4} \frac{V}{K})$		-1.562	↘ <b>-1.563</b> ↗	-1.514	↗ <b>-1.322</b> ↗	-1.321
ZT		0.999	↗ <b>1</b> ↘	0.939	↘ <b>0.715</b> ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.930	<b>1</b>	1.653	<b>3.290</b>	3.296
$VC(10^{-4} \frac{V}{K})$		0.422	↘ $2.14 \times 10^{-5}$ ↘	-0.466	↘ <b>-1.105</b> ↘	-1.106
$T_s(10^{-4} \frac{V}{K})$		-0.092	↗ $-3.22 \times 10^{-5}$ ↗	0.699	↗ <b>1.657</b> ↗	1.660
Pt ( $10^{-3}V$ )		-2.348	↘ -2.350 ↗	-2.277	↗ -1.987 ↗	-1.986

In the degenerate Sn-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T=15.1525 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	5	<b>4.4794468</b>	4	<b>3.6507193</b>	3.65
$\xi_n$	↘	2.271	<b>1.8138</b>	1.364	<b>1</b>	0.999
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.524 ↘	<b>-1.563</b> ↗	-1.502 ↗	<b>-1.322</b> ↗	-1.321
ZT	↗ ↘	0.951 ↗	<b>1</b> ↘	0.923 ↘	<b>0.715</b> ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.638	<b>1</b>	1.768	<b>3.290</b>	3.295
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.353 ↘	$-2.06 \times 10^{-5}$ ↘	-0.530 ↘	<b>-1.105</b> ↘	-1.106
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.529 ↗	$3.08 \times 10^{-5}$ ↗	0.796 ↗	<b>1.657</b> ↗	1.659
$Pt(10^{-3}V)$	↘ ↗	-2.310 ↘	-2.368 ↗	-2.275 ↗	-2.003 ↗	-2.002

For x=0.5,

In the degenerate P-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T=11.4883 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	3	<b>2.7382966</b>	2.5	<b>2.2316667</b>	2.23
$\xi_n$	↘	2.191	<b>1.8138</b>	1.452	<b>1</b>	0.997
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.535 ↘	<b>-1.563</b> ↗	-1.525 ↗	<b>-1.322</b> ↗	-1.319
ZT	↗ ↘	0.965 ↗	<b>1</b> ↘	0.952 ↘	<b>0.715</b> ↘	0.713
$(ZT)_{\text{Mott}}$	↗	0.685	<b>1</b>	1.561	<b>3.290</b>	3.310
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.303 ↘	$3.95 \times 10^{-5}$ ↘	-0.411 ↘	<b>-1.105</b> ↘	-1.110
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.454 ↗	$-5.92 \times 10^{-5}$ ↗	0.616 ↗	<b>1.657</b> ↗	1.665
$Pt(10^{-3}V)$	↘ ↗	-1.764 ↘	-1.796 ↗	-1.752 ↗	-1.518 ↗	-1.516

In the degenerate As-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T=13.9822 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4	<b>3.6766266</b>	3.5	<b>2.99641842</b>	2.99
$\xi_n$	↘	2.162	<b>1.8138</b>	1.617	<b>1</b>	0.991
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.539 ↘	<b>-1.563</b> ↗	-1.553 ↗	<b>-1.322</b> ↗	-1.315
ZT	↗ ↘	0.970 ↗	<b>1</b> ↘	0.987 ↘	<b>0.715</b> ↘	0.708
$(ZT)_{\text{Mott}}$	↗	0.704	<b>1</b>	1.258	<b>3.290</b>	3.348
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.283 ↘	$-7.62 \times 10^{-6}$ ↘	-0.207 ↘	<b>-1.105</b> ↘	-1.120
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.424 ↗	$1.14 \times 10^{-5}$ ↗	0.310 ↗	<b>1.657</b> ↗	1.680
$Pt(10^{-3}V)$	↘ ↗	-2.152 ↘	-2.185 ↗	-2.171 ↗	-1.848 ↗	-1.839

In the degenerate Sb-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for T=16.4055 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	5	<b>4.6727606</b>	4	<b>3.8082485</b>	3.80
$\xi_n$	↘	2.092	<b>1.8138</b>	1.197	<b>1</b>	0.991
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.547 ↘	<b>-1.563</b> ↗	-1.437 ↗	<b>-1.322</b> ↗	-1.315
ZT	↗ ↘	0.980 ↗	<b>1</b> ↘	0.845 ↘	<b>0.715</b> ↘	0.708
$(ZT)_{\text{Mott}}$	↗	0.752	<b>1</b>	2.296	<b>3.290</b>	3.348
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.234 ↘	$6.02 \times 10^{-6}$ ↘	-0.780 ↘	<b>-1.105</b> ↘	-1.120

$T_s (10^{-4} \frac{V}{K})$	-0.350	↗	$-9.03 \times 10^{-6}$	↗	1.171	↗	<b>1.657</b>	↗	1.680
Pt ( $10^{-3}V$ )	-2.538	↘	-2.564	↗	-2.357	↗	-2.168	↗	-2.158

In the degenerate Sn-  $InSb_{1-x}As_x$  alloy, for T=16.535 K one gets:

$N(10^{16}cm^{-3})$	↘	5	<b>4.7282496</b>		4		<b>3.8534551</b>		3.85	
$\xi_n$	↘	2.042	<b>1.8138</b>		1.150		<b>1</b>		0.996	
$S (10^{-4} \frac{V}{K})$		-1.552	↘	<b>-1.563</b>	↗	-1.414	↗	<b>-1.322</b>	↗	-1.319
ZT		0.986	↗	<b>1</b>	↘	0.818	↘	<b>0.715</b>	↘	0.712
$(ZT)_{Mott}$	↗	0.788		<b>1</b>		2.488		<b>3.290</b>		3.314
$VC (10^{-4} \frac{V}{K})$		0.197	↘	$2.73 \times 10^{-5}$	↘	-0.855	↘	<b>-1.105</b>	↘	-1.111
$T_s (10^{-4} \frac{V}{K})$		-0.295	↗	$-4.09 \times 10^{-5}$	↗	1.283	↗	<b>1.657</b>	↗	1.667
Pt ( $10^{-3}V$ )		-2.566	↘	-2.584	↗	-2.337	↗	-2.185	↗	-2.181

For x=1,

In the degenerate P-  $InSb_{1-x}As_x$  alloy, for T=12.633 K, one gets:

$N(10^{16}cm^{-3})$	↘	3	<b>2.9111922</b>		2.5		<b>2.37260017</b>		2.37	
$\xi_n$	↘	1.936	<b>1.8138</b>		1.209		<b>1</b>		0.995	
$S (10^{-4} \frac{V}{K})$		-1.560	↘	<b>-1.563</b>	↗	-1.443	↗	<b>-1.322</b>	↗	-1.318
ZT		0.996	↗	<b>1</b>	↘	0.852	↘	<b>0.715</b>	↘	0.712
$(ZT)_{Mott}$	↗	0.878		<b>1</b>		2.249		<b>3.290</b>		3.319
$VC (10^{-4} \frac{V}{K})$		0.110	↘	$-2.46 \times 10^{-4}$	↘	-0.761	↘	<b>-1.105</b>	↘	-1.113
$T_s (10^{-4} \frac{V}{K})$		-0.165	↗	$3.69 \times 10^{-4}$	↗	1.141	↗	<b>1.657</b>	↗	1.669
Pt ( $10^{-3}V$ )		-1.970	↘	-1.974	↘	-1.823	↗	-1.669	↗	-1.665

In the degenerate As-  $InSb_{1-x}As_x$  alloy, for T=15.3737 K, one gets:

$N(10^{16}cm^{-3})$	↘	4	<b>3.9087682</b>		3.5		<b>3.18559</b>		3.18	
$\xi_n$	↘	1.907	<b>1.8138</b>		1.375		<b>1</b>		0.993	
$S (10^{-4} \frac{V}{K})$		-1.561	↘	<b>-1.563</b>	↗	-1.505	↗	<b>-1.322</b>	↗	-1.317
ZT		0.997	↗	<b>1</b>	↘	0.927	↘	<b>0.715</b>	↘	0.710
$(ZT)_{Mott}$	↗	0.904		<b>1</b>		1.740		<b>3.290</b>		3.337
$VC (10^{-4} \frac{V}{K})$		0.086	↘	$2.66 \times 10^{-5}$	↘	-0.515	↘	<b>-1.105</b>	↘	-1.117
$T_s (10^{-4} \frac{V}{K})$		-0.129	↗	$-4.00 \times 10^{-5}$	↗	0.773	↗	<b>1.657</b>	↗	1.676
Pt ( $10^{-3}V$ )		-2.400	↘	-2.403	↗	-2.313	↗	-2.032	↗	-2.024

In the degenerate Sb-  $InSb_{1-x}As_x$  alloy, for T=18.0385 K, one gets:

$N(10^{16}cm^{-3})$	↘	5.5	<b>4.9677978</b>		4.5		<b>4.0487165</b>		4.045	
$\xi_n$	↘	2.236	<b>1.8138</b>		1.420		<b>1</b>		0.996	
$S (10^{-4} \frac{V}{K})$		-1.529	↘	<b>-1.563</b>	↗	-1.517	↗	<b>-1.322</b>	↗	-1.319

ZT	0.957 ↗	<b>1</b>	↘	0.942 ↘	<b>0.715</b>	↘	0.712
$(ZT)_{Mott}$ ↗	0.658	<b>1</b>	1.630	<b>3.290</b>	3.314		
$VC \left(10^{-4} \frac{V}{K}\right)$	0.331 ↘	$-1.36 \times 10^{-5}$ ↘	-0.452 ↘	<b>-1.105</b> ↘	-1.111		
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.497 ↗	$2.04 \times 10^{-5}$ ↗	0.679 ↗	<b>1.657</b> ↗	1.667		
$Pt (10^{-3}V)$	-2.759 ↘	-2.819 ↗	-2.737 ↗	-2.384 ↗	-2.379		

In the degenerate Sn-  $InSb_{1-x}As_x$  alloy, for T=18.1809 K, one gets:

$N(10^{16}cm^{-3})$	↘	5.5	<b>5.0267904</b>	4.5	<b>4.0967788</b>	4.096	
$\xi_p$	↘	2.186	<b>1.8138</b>	1.374	<b>1</b>	0.999	
$S \left(10^{-4} \frac{V}{K}\right)$	-1.536 ↘	<b>-1.563</b> ↗	-1.505 ↗	<b>-1.322</b> ↗	-1.321		
ZT	0.966 ↗	<b>1</b>	↘	0.927 ↘	<b>0.715</b>	↘	0.714
$(ZT)_{Mott}$ ↗	0.689	<b>1</b>	1.742	<b>3.290</b>	3.295		
$VC \left(10^{-4} \frac{V}{K}\right)$	0.299 ↘	$6.15 \times 10^{-6}$ ↘	-0.516 ↘	<b>-1.105</b> ↘	-1.106		
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.448 ↗	$-9.23 \times 10^{-6}$ ↗	0.775 ↗	<b>1.657</b> ↗	1.659		
$Pt (10^{-3}V)$	-2.793 ↘	-2.842 ↗	-2.735 ↗	-2.403 ↗	-2.402		

**Table 6p.** Here, for a given T and with decreasing N, the reduced Fermi-energy  $\xi_p$  decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T: (i) for  $\xi_p \approx 1.8138$ , while the numerical results of S present a same minimum  $(S)_{min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$ , those of ZT show a same maximum  $(ZT)_{max.} = 1$ , (ii) for  $\xi_p = 1$ , those of S, ZT,  $(ZT)_{Mott}$ , VC, and  $T_s$  present the same results:  $-1.322 \times 10^{-4} \frac{V}{K}$ , 0.715, 3.290,  $-1.105 \times 10^{-4} \frac{V}{K}$ , and  $1.657 \times 10^{-4} \frac{V}{K}$ , respectively, and (iii) for  $\xi_p \approx 1.8138$ ,  $(ZT)_{Mott} = 1$ .

For x=0,

In the degenerate Ga-  $InSb_{1-x}As_x$  alloy, for T=52.183 K, one gets:

$N(10^{18}cm^{-3})$	↘	2.5	<b>2.2902686</b>	2	<b>1.8665455</b>	1.866	
$\xi_p$	↘	2.176	<b>1.8138</b>	1.276	<b>1</b>	0.999	
$S \left(10^{-4} \frac{V}{K}\right)$	-1.537 ↘	<b>-1.563</b> ↗	-1.471 ↗	<b>-1.322</b> ↗	-1.321		
ZT	0.968 ↗	<b>1</b>	↘	0.886 ↘	<b>0.715</b>	↘	0.714
$(ZT)_{Mott}$ ↗	0.695	<b>1</b>	2.021	<b>3.290</b>	3.298		
$VC \left(10^{-4} \frac{V}{K}\right)$	0.292 ↘	$1.35 \times 10^{-6}$ ↘	-0.659 ↘	<b>-1.105</b> ↘	-1.107		
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.438 ↗	$-2.03 \times 10^{-6}$ ↗	0.988 ↗	<b>1.657</b> ↗	1.660		
$Pt (10^{-3}V)$	-8.023 ↘	-8.156 ↗	-7.676 ↗	-6.897 ↗	-6.893		

In the degenerate Mg-  $InSb_{1-x}As_x$  alloy, for T=59.722 K, one gets:

$N(10^{18}cm^{-3})$	↘	3	<b>2.8041452</b>	2.5	<b>2.2853372</b>	2.28
$\xi_p$	↘	2.091	<b>1.8138</b>	1.358	<b>1</b>	0.990



$S \left(10^{-4} \frac{V}{K}\right)$	-1.547	↘	<b>-1.563</b>	↗	-1.500	↗	<b>-1.322</b>	↗	-1.315
ZT	0.980	↗	<b>1</b>	↘	0.921	↘	<b>0.715</b>	↘	0.708
$(ZT)_{Mott}$	↗ 0.752		<b>1</b>		1.784		<b>3.290</b>		3.353
$VC \left(10^{-4} \frac{V}{K}\right)$	0.233	↘	<b><math>2.86 \times 10^{-5}</math></b>	↘	-0.539	↘	<b>-1.105</b>	↘	-1.121
$T_s \left(10^{-4} \frac{V}{K}\right)$	<b>-0.350</b>	↗	<b><math>-4.30 \times 10^{-5}</math></b>	↗	0.809	↗	<b>1.657</b>	↗	1.682
Pt ( $10^{-3}V$ )	-9.241	↘	-9.334	↗	-8.956	↗	-7.893	↗	-7.853

In the degenerate In-  $InSb_{1-x}As_x$  alloy, for T=60.135 K, one gets:

$N(10^{18}cm^{-3})$	↘ 3		<b>2.8332018</b>		2.5		<b>2.30904345</b>		2.305
$\xi_p$	↘ 2.048		<b>1.8138</b>		1.317		<b>1</b>		0.993
$S \left(10^{-4} \frac{V}{K}\right)$	-1.551	↘	<b>-1.563</b>	↗	-1.486	↗	<b>-1.322</b>	↗	-1.317
ZT	0.985	↗	<b>1</b>	↘	0.904	↘	<b>0.715</b>	↘	0.710
$(ZT)_{Mott}$	↗ 0.784		<b>1</b>		1.896		<b>3.290</b>		3.337
$VC \left(10^{-4} \frac{V}{K}\right)$	0.201	↘	<b><math>-2.68 \times 10^{-5}</math></b>	↘	-0.598	↘	<b>-1.105</b>	↘	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$	<b>-0.301</b>	↗	<b><math>4.02 \times 10^{-5}</math></b>	↗	0.897	↗	<b>1.657</b>	↗	1.676
Pt ( $10^{-3}V$ )	-9.330	↘	-9.399	↗	-8.937	↗	-7.948	↗	-7.918

In the degenerate Cd-  $InSb_{1-x}As_x$  alloy, for T=60.558 K, one gets:

$N(10^{18}cm^{-3})$	↘ 3		<b>2.8631806</b>		2.5		<b>2.3334658</b>		2.333
$\xi_p$	↘ 2.004		<b>1.8138</b>		1.275		<b>1</b>		0.994
$S \left(10^{-4} \frac{V}{K}\right)$	-1.555	↘	<b>-1.563</b>	↗	-1.471	↗	<b>-1.322</b>	↗	-1.317
ZT	0.990	↗	<b>1</b>	↘	0.885	↘	<b>0.715</b>	↘	0.710
$(ZT)_{Mott}$	↗ 0.819		<b>1</b>		2.022		<b>3.290</b>		3.330
$VC \left(10^{-4} \frac{V}{K}\right)$	0.167	↘	<b><math>-4.87 \times 10^{-6}</math></b>	↘	-0.659	↘	<b>-1.105</b>	↘	-1.115
$T_s \left(10^{-4} \frac{V}{K}\right)$	<b>-0.250</b>	↗	<b><math>7.30 \times 10^{-6}</math></b>	↗	0.989	↗	<b>1.657</b>	↗	1.673
Pt ( $10^{-3}V$ )	-9.418	↘	-9.465	↗	-8.907	↗	-8.004	↗	-7.978

For x=0.5,

In the degenerate Ga-  $InSb_{1-x}As_x$  alloy, for T=52.449 K, one gets:

$N(10^{18}cm^{-3})$	↘ 2		<b>1.8889296</b>		1.7		<b>1.53945142</b>		1.539
$\xi_p$	↘ 2.048		<b>1.8138</b>		1.395		<b>1</b>		0.999
$S \left(10^{-4} \frac{V}{K}\right)$	-1.551	↘	<b>-1.563</b>	↗	-1.511	↗	<b>-1.322</b>	↗	-1.321
ZT	0.985	↗	<b>1</b>	↘	0.934	↘	<b>0.715</b>	↘	0.714
$(ZT)_{Mott}$	↗ 0.784		<b>1</b>		1.690		<b>3.290</b>		3.298
$VC \left(10^{-4} \frac{V}{K}\right)$	0.201	↘	<b><math>2.37 \times 10^{-5}</math></b>	↘	-0.487	↘	<b>-1.105</b>	↘	-1.107
$T_s \left(10^{-4} \frac{V}{K}\right)$	<b>-0.301</b>	↗	<b><math>-3.55 \times 10^{-5}</math></b>	↗	0.731	↗	<b>1.657</b>	↗	1.660
Pt ( $10^{-2}V$ )	-0.814	↘	-0.820	↗	-0.792	↗	-0.6932	↗	-0.6928

In the degenerate Mg-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $T=60.028$  K, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	<b>2.3127562</b>	↗	2.2	<b>1.88488252</b>	↘	1.88
$\xi_p$	↘	2.134	<b>1.8138</b>	↗	1.614	<b>1</b>	↘	0.989
$S(10^{-4}\frac{V}{K})$	↘	-1.542	<b>-1.563</b>	↗	-1.552	<b>-1.322</b>	↘	-1.314
ZT	↗	0.974	<b>1</b>	↘	0.986	<b>0.715</b>	↘	0.707
$(ZT)_{\text{Mott}}$	↗	0.722	<b>1</b>	↘	1.263	<b>3.290</b>	↘	3.360
$VC(10^{-4}\frac{V}{K})$	↘	0.264	<b><math>-2.497 \times 10^{-5}</math></b>	↗	-0.210	<b>-1.105</b>	↘	-1.123
$T_s(10^{-4}\frac{V}{K})$	↘	-0.396	<b><math>3.73 \times 10^{-5}</math></b>	↗	0.316	<b>1.657</b>	↘	1.684
Pt ( $10^{-2}V$ )	↘	-0.926	<b>-0.938</b>	↗	-0.932	<b>-0.79339</b>	↘	-0.7889

In the degenerate In-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $T=60.442K$ , one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	<b>2.336721</b>	↗	2.2	<b>1.9044144</b>	↘	1.904
$\xi_p$	↘	2.091	<b>1.8138</b>	↗	1.573	<b>1</b>	↘	0.999
$S(10^{-4}\frac{V}{K})$	↘	-1.547	<b>-1.563</b>	↗	-1.547	<b>-1.322</b>	↘	-1.321
ZT	↗	0.980	<b>1</b>	↘	0.980	<b>0.715</b>	↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.752	<b>1</b>	↘	1.329	<b>3.290</b>	↘	3.296
$VC(10^{-4}\frac{V}{K})$	↘	0.233	<b><math>-2.67 \times 10^{-5}</math></b>	↗	-0.258	<b>-1.105</b>	↘	-1.106
$T_s(10^{-4}\frac{V}{K})$	↘	-0.350	<b><math>4.01 \times 10^{-5}</math></b>	↗	0.387	<b>1.657</b>	↘	1.660
Pt ( $10^{-2}V$ )	↘	-0.935	<b>-0.945</b>	↗	-0.935	<b>-0.7989</b>	↘	-0.7985

In the degenerate Cd-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $T=60.8672K$ , one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	<b>2.3614464</b>	↗	2.2	<b>1.9245578</b>	↘	1.924
$\xi_p$	↘	2.047	<b>1.8138</b>	↗	1.531	<b>1</b>	↘	0.999
$S(10^{-4}\frac{V}{K})$	↘	-1.552	<b>-1.563</b>	↗	-1.541	<b>-1.322</b>	↘	-1.321
ZT	↗	0.985	<b>1</b>	↘	0.972	<b>0.715</b>	↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.785	<b>1</b>	↘	1.403	<b>3.290</b>	↘	3.298
$VC(10^{-4}\frac{V}{K})$	↘	0.200	<b><math>-6.78 \times 10^{-6}</math></b>	↗	-0.309	<b>-1.105</b>	↘	-1.107
$T_s(10^{-4}\frac{V}{K})$	↘	-0.300	<b><math>1.02 \times 10^{-5}</math></b>	↗	0.463	<b>1.657</b>	↘	1.660
Pt ( $10^{-2}V$ )	↘	-0.944	<b>-0.951</b>	↗	-0.938	<b>-0.80448</b>	↘	-0.80398

For  $x=1$ ,

In the degenerate Ga-  $\text{InSb}_{1-x}\text{As}_x$  alloy, for  $T=52.177$  K, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2	<b>1.4873359</b>	↗	1.45	<b>1.21215745</b>	↘	1.21
$\xi_p$	↘	3.120	<b>1.8138</b>	↗	1.712	<b>1</b>	↘	0.993
$S(10^{-4}\frac{V}{K})$	↘	-1.358	<b>-1.563</b>	↗	-1.560	<b>-1.322</b>	↘	-1.316
ZT	↗	0.755	<b>1</b>	↘	0.997	<b>0.715</b>	↘	0.709
$(ZT)_{\text{Mott}}$	↗	0.338	<b>1</b>	↘	1.123	<b>3.290</b>	↘	3.338
$VC(10^{-4}\frac{V}{K})$	↘	0.639	<b><math>2.66 \times 10^{-5}</math></b>	↗	-0.103	<b>-1.105</b>	↘	-1.117

$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.958	$\nearrow -3.99 \times 10^{-5}$	$\nearrow$	0.154	$\nearrow$	<b>1.657</b>	$\nearrow$	1.676	
Pt ( $10^{-2}V$ )	-0.709	$\searrow$	-0.815	$\nearrow$	-0.814	$\nearrow$	-0.6896	$\nearrow$	-0.6869

In the degenerate Mg-  $InSb_{1-x}As_x$  alloy, for T=59.716 K, one gets:

$N(10^{18}cm^{-3})$	$\searrow$	2.5	<b>1.8210554</b>	1.6	<b>1.4841384</b>	1.484				
$\xi_p$	$\searrow$	3.218	<b>1.8138</b>	1.300	<b>1</b>	0.999				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.337	$\searrow$	<b>-1.563</b>	$\nearrow$	-1.480	$\nearrow$	<b>-1.322</b>	$\nearrow$	-1.321
ZT		0.732	$\nearrow$	<b>1</b>	$\searrow$	0.897	$\searrow$	<b>0.715</b>	$\searrow$	0.7148
$(ZT)_{Mott}$	$\nearrow$	0.318		<b>1.0009</b>		1.946		<b>3.290</b>		3.292
$VC \left(10^{-4} \frac{V}{K}\right)$		0.645	$\searrow$	$1.17 \times 10^{-5}$	$\searrow$	-0.623	$\searrow$	<b>-1.105</b>	$\searrow$	-1.1056
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.968	$\nearrow$	$-1.76 \times 10^{-5}$	$\nearrow$	0.934	$\nearrow$	<b>1.657</b>	$\nearrow$	1.658
Pt ( $10^{-2}V$ )		-0.798	$\searrow$	-0.933	$\nearrow$	-0.884	$\nearrow$	-0.7893	$\nearrow$	-0.7891

In the degenerate In-  $InSb_{1-x}As_x$  alloy, for T=60.128 K, one gets:

$N(10^{18}cm^{-3})$	$\searrow$	2.5	<b>1.8399251</b>	1.6	<b>1.499519795</b>	1.498				
$\xi_p$	$\searrow$	3.169	<b>1.8138</b>	1.259	<b>1</b>	0.996				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.348	$\searrow$	<b>-1.563</b>	$\nearrow$	-1.464	$\nearrow$	<b>-1.322</b>	$\nearrow$	-1.319
ZT		0.743	$\nearrow$	<b>1</b>	$\searrow$	0.878	$\searrow$	<b>0.715</b>	$\searrow$	0.712
$(ZT)_{Mott}$	$\nearrow$	0.327		<b>1</b>		2.074		<b>3.290</b>		3.317
$VC \left(10^{-4} \frac{V}{K}\right)$		0.643	$\searrow$	$2.54 \times 10^{-6}$	$\searrow$	-0.684	$\searrow$	<b>-1.105</b>	$\searrow$	-1.112
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.964	$\nearrow$	$-3.81 \times 10^{-6}$	$\nearrow$	1.026	$\nearrow$	<b>1.657</b>	$\nearrow$	1.668
Pt ( $10^{-2}V$ )		-0.810	$\searrow$	-0.940	$\nearrow$	-0.880	$\nearrow$	-0.795	$\nearrow$	-0.793

In the degenerate Cd-  $InSb_{1-x}As_x$  alloy, for T=60.552 K, one gets:

$N(10^{18}cm^{-3})$	$\searrow$	2.5	<b>1.8593938</b>	1.6	<b>1.51539518</b>	1.515				
$\xi_p$	$\searrow$	3.119	<b>1.8138</b>	1.217	<b>1</b>	0.999				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.358	$\searrow$	<b>-1.563</b>	$\nearrow$	-1.445	$\nearrow$	<b>-1.322</b>	$\nearrow$	-1.321
ZT		0.755	$\nearrow$	<b>1</b>	$\searrow$	0.856	$\searrow$	<b>0.715</b>	$\searrow$	0.714
$(ZT)_{Mott}$	$\nearrow$	0.338		<b>1</b>		2.219		<b>3.290</b>		3.297
$VC \left(10^{-4} \frac{V}{K}\right)$		0.639	$\searrow$	$-2.58 \times 10^{-5}$	$\searrow$	-0.748	$\searrow$	<b>-1.105</b>	$\searrow$	-1.107
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.958	$\nearrow$	$3.87 \times 10^{-5}$	$\nearrow$	0.112	$\nearrow$	<b>1.657</b>	$\nearrow$	1.660
Pt ( $10^{-2}V$ )		-0.822	$\searrow$	-0.946	$\nearrow$	-0.876	$\nearrow$	-0.800	$\nearrow$	-0.7998