



ELECTRICAL-AND-THERMOELECTRIC PROPERTIES, OBTAINED IN N(P)-TYPE DEGENERATE $\text{InSb}_{(1-x)}\text{As}_x$ -CRYSTALLINE ALLOY

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Article Received on 08/12/2024

Article Revised on 28/12/2024

Article Accepted on 18/01/2025



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ABSTRACT

In the $n^+(p^+) - p(n)$ $\text{InSb}_{1-x}\text{As}_x$ -crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018; Van Cong et al.,1984), are now revised and performed, by basing on our basic expressions, given Equations (1, 3, 5, 7, 11, 14, 19). Some remarkable results could be cited in the following. In Tables 5n (5p) given Appendix 1, for a given impurity density N and with increasing temperature T , and then in Tables 6n(6p) given Appendix 1, for a given T and with decreasing N , the reduced Fermi-energy $\xi_{n(p)}$ decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). Further, one notes in these Tables that with increasing T (or with decreasing N) one obtains: (i) for $\xi_{n(p)} \simeq 1.8138$, while the numerical results of the Seebeck coefficient S present a same

minimum $(S)_{\min.} (\simeq -1.563 \times 10^{-4} \frac{V}{K})$, those of the figure of merit ZT show a same maximum $(ZT)_{\max.} = 1$, (ii) for $\xi_{n(p)} = 1$, S , ZT , the Mott figure of merit $(ZT)_{\text{Mott}}$, the Van-Cong coefficient VC , and the Thomson coefficient Ts present the same results: $-1.322 \times 10^{-4} \frac{V}{K}$, 0.715, 3.290, $-1.105 \times 10^{-4} \frac{V}{K}$, and $1.657 \times 10^{-4} \frac{V}{K}$, respectively, and (iii) for $\xi_n \simeq 1.8138$, $(ZT)_{\text{Mott}} = 1$. It seems that these same results could present a new law in the thermoelectric properties, obtained in the degenerate case.

KEYWORDS: Electrical conductivity, Seebeck coefficient, Figure of merit, Van-Cong coefficient, Thomson coefficient, Peltier coefficient.

INTRODUCTION

In the $n^+(p^+) - p(n)$ $\text{InSb}_{1-x}\text{As}_x$ - crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018; Van Cong et al.,1984), are now revised and performed, by basing on our following basic expressions (Van Cong, 1980 and 2024; Van Cong and Debiais, 1993; Van Cong and Doan Khanh, 1992).

(1) The effective extrinsic static dielectric constant law, $\varepsilon(r_{d(a)}, x)$, due to the impurity size effect, is determined in Eq. (1).

(2) The generalized Mott criterium in the metal-insulator transition is expressed in Equations (3, 5, 6), showing that $N_{\text{CDn(CDp)}}$ is just **the density of electrons (holes) localized in the exponential conduction (valence)-band tail**, $N_{\text{CDn(CDp)}}^{\text{EBT}}$, with a precision of the order of 2.86×10^{-7} , as given in our recent work (Van Cong, 2024), and the effective electron (hole)-density: $N^* \equiv N - N_{\text{CDn(CDp)}} \simeq N - N_{\text{CDn(CDp)}}^{\text{EBT}}$, as that observed in the compensated crystals.

(3) The ratio of the inverse effective screening length $k_{\text{sn(sp)}}$ to Fermi wave number $k_{\text{Fn(kp)}}$ at 0 K, $R_{\text{sn(sp)}}(N^*)$, defined in Eq. (7), is valid at any density N^* .

(4) The Fermi energy for any N and T, $E_{\text{Fn(Fp)}}$, determined in Eq. (11) with a precision of the order of 2.11×10^{-4} (Van Cong, 1993), and it is present in all the expressions of electrical-and-thermoelectric coefficients.

(v) Our expressions for the electrical conductivity, σ , and for the Seebeck coefficient, S, determined respectively in Equations (14, 19) are the basic expressions for determining the following electrical-and-thermoelectric coefficients.

OUR STATIC DIELECTRIC CONSTANT LAW-AND-GENERALIZED MOTT CRITERIUM IN THE METAL-INSULATOR TRANSITION

First of all, in the $n^+(p^+) - p(n)$ $\text{X(x)} \equiv \text{InSb}_{1-x}\text{As}_x$ - crystalline alloy at T=0 K, we denote the donor (acceptor) d(a)-radius by $r_{d(a)}$, the corresponding intrinsic one by: $r_{\text{do(ao)}} = r_{\text{Sb(In)}}$,

the unperturbed relative effective electron (hole) mass in conduction (valence) bands by: $m_{c(v)}(\mathbf{x})/m_o$, the unperturbed relative static dielectric constant by: $\epsilon_o(\mathbf{x})$. Then, their values are reported in **Table 1 in Appendix 1**.

Therefore, we can define the effective donor (acceptor)-ionization energy in absolute values as:

$$E_{do(ao)}(\mathbf{x}) = \frac{13600 \times [m_{c(v)}(\mathbf{x})/m_o]}{[\epsilon_o(\mathbf{x})]^2} \text{ meV} , \text{ and then, the isothermal bulk modulus, by:}$$

$$B_{do(ao)}(\mathbf{x}) \equiv \frac{E_{do(ao)}(\mathbf{x})}{\left(\frac{4\pi}{3}\right) \times (r_{do(ao)})^3} .$$

Effect of Impurity $r_{d(a)}$ -size, with a given \mathbf{x}

Here, the changes in all the energy-band-structure parameters, expressed in terms of the effective relative dielectric constant $\epsilon(r_{d(a)}, \mathbf{x})$, developed as follows.

At $r_{d(a)} = r_{do(ao)}$, the needed boundary conditions are found to be, for the impurity-atom volume $V = (4\pi/3) \times (r_{d(a)})^3$, $V_{do(ao)} = (4\pi/3) \times (r_{do(ao)})^3$, for the pressure p , $p_o = 0$, and for the deformation potential energy (or the strain energy) σ , $\sigma_o = 0$. Further, the two important equations (Van Cong, 1984 and 2018), used to determine the σ -variation, $\Delta\sigma \equiv \sigma - \sigma_o = \sigma$, are defined by: $\frac{dp}{dV} = -\frac{B}{V}$ and $p = -\frac{d\sigma}{dV}$. giving: $\frac{d}{dV}\left(\frac{d\sigma}{dV}\right) = \frac{B}{V}$. Then, by an integration, one gets:

$$\left[\Delta\sigma(r_{d(a)}, \mathbf{x})\right]_{n(p)} = B_{do(ao)}(\mathbf{x}) \times (V - V_{do(ao)}) \times \ln\left(\frac{V}{V_{do(ao)}}\right) = E_{do(ao)}(\mathbf{x}) \times \left[\left(\frac{r_{d(a)}}{r_{do(ao)}}\right)^3 - 1\right] \times \ln\left(\frac{r_{d(a)}}{r_{do(ao)}}\right)^3 \geq 0.$$

Furthermore, we also shown that, as $r_{d(a)} > r_{do(ao)}$ ($r_{d(a)} < r_{do(ao)}$), the compression (dilatation) gives rise to the increase (the decrease) in the energy gap $E_{gn(gp)}(r_{d(a)}, \mathbf{x})$, and the effective donor (acceptor)-ionization energy $E_{d(a)}(r_{d(a)}, \mathbf{x})$ in absolute values, obtained in the effective Bohr model, which is represented respectively by: $\pm [\Delta\sigma(r_{d(a)}, \mathbf{x})]_{n(p)}$,

$$E_{gno(gp_o)}(r_{d(a)}, \mathbf{x}) - E_{go}(\mathbf{x}) = E_{d(a)}(r_{d(a)}, \mathbf{x}) - E_{do(ao)}(\mathbf{x}) = E_{do(ao)}(\mathbf{x}) \times \left[\left(\frac{\epsilon_o(\mathbf{x})}{\epsilon(r_{d(a)})}\right)^2 - 1 \right] + [\Delta\sigma(r_{d(a)}, \mathbf{x})]_{n(p)} ,$$

for $r_{d(a)} \geq r_{do(ao)}$, and for $r_{d(a)} \leq r_{do(ao)}$,

$$E_{\text{gno}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d(a)}}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{do(ao)}}(\mathbf{x}) = E_{\text{do(ao)}}(\mathbf{x}) \times \left[\left(\frac{\epsilon_0(\mathbf{x})}{\epsilon(r_{\text{d(a)}, \mathbf{x}})} \right)^2 - 1 \right] = - [\Delta\sigma(r_{\text{d(a)}, \mathbf{x}})]_{\text{n(p)}}$$

Therefore, one obtains the expressions for relative dielectric constant $\epsilon(r_{\text{d(a)}, \mathbf{x}}$) and energy band gap $E_{\text{gn}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}$), as:

(i)-for $r_{\text{d(a)}} \geq r_{\text{do(ao)}}$, since $\epsilon(r_{\text{d(a)}, \mathbf{x}}) = \frac{\epsilon_0(\mathbf{x})}{\sqrt{1 + \left[\left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 - 1 \right] \times \ln \left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3}} \leq \epsilon_0(\mathbf{x})$, being a **new**

$\epsilon(r_{\text{d(a)}, \mathbf{x}}$)-law,

$$E_{\text{gno}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d(a)}}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{do(ao)}}(\mathbf{x}) = E_{\text{do(ao)}}(\mathbf{x}) \times \left[\left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 - 1 \right] \times \ln \left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 \geq 0, \tag{1a}$$

according to the increase in both $E_{\text{gn}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}$) and $E_{\text{d(a)}}(r_{\text{d(a)}, \mathbf{x}}$), with increasing $r_{\text{d(a)}}$ and for a given \mathbf{x} , and

(ii)-for $r_{\text{d(a)}} \leq r_{\text{do(ao)}}$, since $\epsilon(r_{\text{d(a)}, \mathbf{x}}) = \frac{\epsilon_0(\mathbf{x})}{\sqrt{1 - \left[\left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 - 1 \right] \times \ln \left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3}} \geq \epsilon_0(\mathbf{x})$, with a

condition, given by: $\left[\left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 - 1 \right] \times \ln \left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 < 1$, being a **new** $\epsilon(r_{\text{d(a)}, \mathbf{x}}$)-law,

$$E_{\text{gno}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{go}}(\mathbf{x}) = E_{\text{d(a)}}(r_{\text{d(a)}, \mathbf{x}}) - E_{\text{do(ao)}}(\mathbf{x}) = -E_{\text{do(ao)}}(\mathbf{x}) \times \left[\left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 - 1 \right] \times \ln \left(\frac{r_{\text{d(a)}}}{r_{\text{do(ao)}}} \right)^3 \leq 0, \tag{1b}$$

corresponding to the decrease in both $E_{\text{gn}(\text{gp})}(r_{\text{d(a)}, \mathbf{x}}$) and $E_{\text{d(a)}}(r_{\text{d(a)}, \mathbf{x}}$), with decreasing $r_{\text{d(a)}}$ and for a given \mathbf{x} ; therefore, the effective Bohr radius $a_{\text{Bn}(\text{Bp})}(r_{\text{d(a)}, \mathbf{x}}$) is defined by:

$$a_{\text{Bn}(\text{Bp})}(r_{\text{d(a)}, \mathbf{x}}) \equiv \frac{\epsilon(r_{\text{d(a)}, \mathbf{x}}) \times \hbar^2}{m_{\text{c(v)}(\mathbf{x})} \times m_0 \times q^2} = 0.53 \times 10^{-8} \text{ cm} \times \frac{\epsilon(r_{\text{d(a)}, \mathbf{x}})}{m_{\text{c(v)}(\mathbf{x})}}. \tag{2}$$

Generalized Mott Criterium in the Metal-Insulator Transition

Furthermore, it is interesting to remark that the critical total donor (acceptor)-density in the metal-insulator transition (MIT) at $T=0$ K, $N_{\text{CDn}(\text{NDp})}(r_{\text{d(a)}, \mathbf{x}}$), was given by the Mott's criterium, with an empirical parameter, $M_{\text{n(p)}}$, as:

$$N_{CDn(CDp)}(r_{d(a)}, x)^{1/3} \times a_{Bn(Bp)}(r_{d(a)}, x) = M_{n(p)}, M_{n(p)} = 0.25, \quad (3)$$

depending thus on our **new** $\varepsilon(r_{d(a)}, x)$ -law.

This excellent one can be explained from the definition of the reduced effective Wigner-Seitz (WS) radius $r_{sn(sp)}$, characteristic of interactions, by:

$$r_{sn(sp)}(N, r_{d(a)}, x) \equiv \left(\frac{3}{4\pi N}\right)^{1/3} \times \frac{1}{a_{Bn(Bp)}(r_{d(a)}, x)} = 1.1723 \times 10^8 \times \left(\frac{1}{N}\right)^{1/3} \times \frac{m_{c(v)}(x) \times m_0}{\varepsilon(r_{d(a)}, x)}, \quad (4)$$

being equal to, in particular, at $N=N_{CDn(CDp)}(r_{d(a)}, x)$: $r_{sn(sp)}(N_{CDn(CDp)}(r_{d(a)}, x), r_{d(a)}, x) = 2.4813963$, for any $(r_{d(a)}, x)$ -values. Then, from Eq. (4), one also has :

$$N_{CDn(CDp)}(r_{d(a)}, x)^{1/3} \times a_{Bn(Bp)}(r_{d(a)}, x) = \left(\frac{3}{4\pi}\right)^{1/3} \times \frac{1}{2.4813963} = 0.25 = (WS)_{n(p)} = M_{n(p)}, \quad (5)$$

explaining thus the existance of the Mott's criterium

Furthermore, by using $M_{n(p)} = 0.25$, according to the empirical Heisenberg parameter $\mathcal{H}_{n(p)} = 0.47137$, as those given in our previous work (Van Cong, 2024), we have also showed that $N_{CDn(CDp)}$ is just **the density of electrons (holes) localized in the exponential conduction (valence)-band tail**, $N_{CDn(CDp)}^{EBT}$, with a precision of the order of 2.86×10^{-7} .

It should be noted that the values of $M_{n(p)}$ and $\mathcal{H}_{n(p)}$ could be chosen so that those of $N_{CDn(CDp)}$ and $N_{CDn(CDp)}^{EBT}$ are in good agreement with their experimental results.

Therefore, the density of electrons (holes) given in parabolic conduction (valence) bands can be defined, as that given in compensated materials, by:

$$N^*(N, r_{d(a)}, x) \equiv N - N_{CDn(NDp)}(r_{d(a)}, x) = N^*, \text{ for a presentation simplicity.} \quad (6)$$

In summary, as observed in Table 1 of our previous paper (Van Cong, 2024), one remarks that, for a given x and an increasing $r_{d(a)}$, $\varepsilon(r_{d(a)}, x)$ decreases, while $E_{gno(gpo)}(r_{d(a)}, x)$, $N_{CDn(NDp)}(r_{d(a)}, x)$ and $N_{CDn(CDp)}^{EBT}(r_{d(a)}, x)$ increase, affecting strongly all the physical properties, as those observed in following Sections.

PHYSICAL MODEL

In the $n^+(p^+) - p(n) X(x) \equiv \text{InSb}_{1-x}\text{As}_x$ - crystalline alloy, if denoting the Fermi wave number by: $k_{Fn(Fp)}(N^*) \equiv \left(\frac{3\pi^2 N^*}{\varepsilon_{c(v)}}\right)^{1/3}$, the reduced effective Wigner-Seitz (WS) radius $r_{sn(sp)}$,

characteristic of interactions, being given in Eq. (4), in which N is replaced by N^* , is now defined by:

$$\gamma \times r_{sn(sp)}(N^*) \equiv \frac{k_{Fn(Fp)}^{-1}}{a_{Bn(Bp)}} < 1,$$

being proportional to $N^{*-1/3}$. Here, $\gamma = (4/9\pi)^{1/3}$, $k_{Fn(Fp)}^{-1}$ means the averaged distance between ionized donors (acceptors), and $a_{Bn(Bp)}(r_{d(a)}, x)$ is determined in Eq. (2).

Then, the ratio of the inverse effective screening length $k_{sn(sp)}$ to Fermi wave number $k_{Fn(kp)}$ at 0 K is defined by:

$$R_{sn(sp)}(N^*) \equiv \frac{k_{sn(sp)}}{k_{Fn(Fp)}} = \frac{k_{Fn(Fp)}^{-1}}{k_{sn(sp)}^{-1}} = R_{snWS(spWS)} + [R_{snTF(spTF)} - R_{snWS(spWS)}]e^{-r_{sn(sp)}} < 1, \quad (7)$$

being valid at any N^*

Here, these ratios, $R_{snTF(spTF)}$ and $R_{snWS(spWS)}$, can be determined as follows.

First, for $N \gg N_{CDn(NDp)}(r_{d(a)}, x)$, according to the **Thomas-Fermi (TF)-approximation**, the ratio $R_{snTF(spTF)}(N^*)$ is reduced to

$$R_{snTF(spTF)}(N^*) \equiv \frac{k_{snTF(spTF)}}{k_{Fn(Fp)}} = \frac{k_{Fn(Fp)}^{-1}}{k_{snTF(spTF)}^{-1}} = \sqrt{\frac{4\gamma r_{sn(sp)}}{\pi}} \ll 1, \quad (8)$$

being proportional to $N^{*-1/6}$.

Secondly, for $N \ll N_{CDn(NDp)}(r_{d(a)})$, according to the **Wigner-Seitz (WS)-approximation**, the ratio $R_{snWS(spWS)}$ is respectively reduced to

$$R_{sn(sp)WS}(N^*) \equiv \frac{k_{sn(sp)WS}}{k_{Fn}} = 0.5 \times \left(\frac{s}{2\pi} - \gamma \frac{d[r_{sn(sp)}^2 \times E_{CE}(N^*)]}{dr_{sn(sp)}} \right), \quad (9)$$

where $E_{CE}(N^*)$ is the majority-carrier correlation energy (CE), being determined by (Van Cong, 2018):

$$E_{CE}(N^*) = \frac{-0.87553}{0.0908 + r_{sn(sp)}} + \frac{\frac{0.87553}{0.0908 + r_{sn(sp)}} + \left(\frac{2[1 - \ln(2)]}{\pi^2}\right) \times \ln(r_{sn(sp)}) - 0.093288}{1 + 0.03847728 \times r_{sn(sp)}^{1.67378876}}.$$

Furthermore, in the highly degenerate case, the physical conditions are found to be given by (Van Cong, 2018)

$$\frac{k_{Fn(Fp)}^{-1}}{a_{Bn(Bp)}} < \frac{\eta_{n(p)}}{E_{Fno(Fpo)}} \equiv \frac{1}{A_{n(p)}} < \frac{k_{Fn(Fp)}^{-1}}{k_{sn(sp)}^{-1}} \equiv R_{sn(sp)} < 1, \quad \eta_{n(p)}(N^*) \equiv \frac{\sqrt{2\pi N^*}}{\varepsilon(r_{d(a)})} \times q^2 k_{sn(sp)}^{-1/2}, \quad (10)$$

which gives: $A_{n(p)}(N^*) = \frac{E_{Fno(Fpo)}(N^*)}{\eta_{n(p)}(N^*)}$.

FERMI ENERGY AND FERMI-DIRAC DISTRIBUTION FUNCTION

Fermi Energy and generalized Einstein relation

Here, for a presentation simplicity, we change all the sign of various parameters, given in the $p^+ - X(x)$ - crystalline alloy in order to obtain the same one, as given in the $n^+ - X(x)$ - crystalline alloy, according to the reduced Fermi energy, $\xi_{n(p)}(N, r_{d(a)}, x, T) \equiv \frac{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}{k_B T} > 0 (< 0)$, obtained respectively in the degenerate (non-degenerate) case.

For any $(N, r_{d(a)}, x, T)$, the reduced Fermi energy $\xi_{n(p)}(N, r_{d(a)}, x, T)$ or the Fermi energy $E_{Fn(Fp)}(N, r_{d(a)}, x, T)$, obtained in our previous paper (Van Cong and Debais, 1993), obtained with a precision of the order of 2.11×10^{-4} , is found to be given by:

$$\xi_{n(p)}(u) \equiv \frac{E_{Fn(Fp)}(u)}{k_B T} = \frac{G(u) + Au^B F(u)}{1 + Au^B} \equiv \frac{V(u)}{W(u)}, A = 0.0005372 \text{ and } B = 4.82842262, \quad (11)$$

where u is the reduced electron density, $u(N, r_{d(a)}, x, T) \equiv \frac{N^+}{N_{c(v)}(T, x)}$,

$$N_{c(v)}(T, x) = 2g_{c(v)} \times \left(\frac{m_{c(v)}(x) \times m_0 \times k_B T}{2\pi \hbar^2} \right)^{\frac{3}{2}} \text{ (cm}^{-3}\text{)}, \quad g_{c(v)} = 1,$$

$$F(u) = au^{\frac{2}{3}} \left(1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}} \right)^{-\frac{2}{3}}, a = [(3\sqrt{\pi}/4)]^{2/3}, b = \frac{1}{8} \left(\frac{\pi}{a} \right)^2, c = \frac{62.3739855}{1920} \left(\frac{\pi}{a} \right)^4, \text{ and}$$

$$G(u) \simeq \text{Ln}(u) + 2^{-\frac{3}{2}} \times u \times e^{-du}; d = 2^{3/2} \left[\frac{1}{\sqrt{27}} - \frac{3}{16} \right] > 0.$$

So, in the non-degenerate case ($u \ll 1$), one has: $E_{Fn(Fp)}(u) = k_B T \times G(u) \simeq k_B T \times \text{Ln}(u)$ as $u \rightarrow 0$, **the limiting condition**, and in the very degenerate case ($u \gg 1$), one gets:

$$E_{Fn(Fp)}(u) = k_B T \times F(u) = k_B T \times au^{\frac{2}{3}} \left(1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}} \right)^{-\frac{2}{3}} \simeq \frac{\hbar^2 \times k_{Fn(Fp)}^2(N^*)}{2 \times m_{c(v)}(x) \times m_0} \text{ as } u \rightarrow \infty,$$

the limiting condition. In other words, $\xi_{n(p)} \equiv \frac{E_{Fn(Fp)}}{k_B T}$ is accurate, and it also verifies the correct limiting conditions. In the following, it will be present in all the electrical-and-thermoelectric coefficients.

In particular, at $T=0K$, since $u^{-1} = 0$, Eq. (11) is reduced to: $E_{Fno(Fpo)}(N^*) \equiv \frac{\hbar^2 \times k_{Fn(Fp)}^2(N^*)}{2 \times m_{c(v)}(x) \times m_0}$, being proportional to $(N^*)^{2/3}$, and also equal to 0, according to the MIT.

In the following, it should be noted that such the accurate expression of $\xi_{n(p)}(N, r_{d(a)}, x, T)$ is present in all the following electrical-and-thermoelectric.

FERMI-DIRAC DISTRIBUTION FUNCTION (FDDF)

The Fermi-Dirac distribution function (FDDF) is given by: $f(E) \equiv (1 + e^\gamma)^{-1}$, $\gamma \equiv (E - E_{Fn(Fp)})/(k_B T)$.

So, the average of E^p , calculated using the FDDF-method, as developed in our previous work (Van Cong, 2018) is found to be given by:

$$\langle E^p \rangle_{FDDF} \equiv G_p(E_{Fn(Fp)}) \times E_{Fn(Fp)}^p \equiv \int_{-\infty}^{\infty} E^p \times \left(-\frac{\partial f}{\partial E} \right) dE, \quad -\frac{\partial f}{\partial E} = \frac{1}{k_B T} \times \frac{e^\gamma}{(1+e^\gamma)^2}.$$

Further, one notes that, at 0 K, $-\frac{\partial f}{\partial E} = \delta(E - E_{Fn(Fp)})$, $\delta(E - E_{Fn(Fp)})$ being the Dirac delta (δ)-function. Therefore, $G_p(E_{Fn(Fp)}) = 1$.

Then, at low T, by a variable change $\gamma \equiv (E - E_{Fn(Fp)})/(k_B T)$, one has:

$$G_p(E_{Fn(Fp)}) \equiv 1 + E_{Fn(Fp)}^{-p} \times \int_{-\infty}^{\infty} \frac{e^\gamma}{(1+e^\gamma)^2} \times (k_B T \gamma + E_{Fn(Fp)})^p d\gamma = 1 + \sum_{\mu=1,2,\dots}^p C_p^\beta \times (k_B T)^\beta \times E_{Fn(Fp)}^{-\beta} \times I_\beta,$$

where $C_p^\beta \equiv p(p - 1) \dots (p - \beta + 1)/\beta!$ and the integral I_β is given by:

$$I_\beta = \int_{-\infty}^{\infty} \frac{\gamma^\beta \times e^\gamma}{(1+e^\gamma)^2} d\gamma = \int_{-\infty}^{\infty} \frac{\gamma^\beta}{(e^{\gamma/2} + e^{-\gamma/2})^2} d\gamma, \text{ vanishing for odd values of } \beta. \text{ Then, for even values of } \beta = 2n, \text{ with } n=1, 2, \dots, \text{ one obtains:}$$

$$I_{2n} = 2 \int_0^{\infty} \frac{\gamma^{2n} \times e^\gamma}{(1+e^\gamma)^2} d\gamma.$$

Now, using an identity $(1 + e^\gamma)^{-2} \equiv \sum_{s=1}^{\infty} (-1)^{s+1} s \times e^{\gamma(s-1)}$, a variable change: $s\gamma = -t$, the Gamma function: $\int_0^{\infty} t^{2n} e^{-t} dt \equiv \Gamma(2n + 1) = (2n)!$, and also the definition of the Riemann's zeta function: $\zeta(2n) \equiv 2^{2n-1} \pi^{2n} |B_{2n}|/(2n)!$, B_{2n} being the Bernoulli numbers, one finally gets: $I_{2n} = (2^{2n} - 2) \times \pi^{2n} \times |B_{2n}|$. So, from Eq. (22), we get in the degenerate case the following ratio:

$$G_p(E_{Fn(Fp)}) \equiv \frac{\langle E^p \rangle_{FDDF}}{E_{Fn(Fp)}^p} = 1 + \sum_{n=1}^p \frac{p(p-1)\dots(p-2n+1)}{(2n)!} \times (2^{2n} - 2) \times |B_{2n}| \times y^{2n} \equiv G_{p \geq 1}(y), \quad (12)$$

$$\text{where } y \equiv \frac{\pi}{\xi_{n(p)}(N^*, T)} = \frac{\pi k_B T}{E_{Fn(Fp)}(N^*, T)}.$$

Then, some usual results of $G_{p \geq 1}(y)$ are given in **Table 2 in Appendix 1, being important ones in this work.**

ELECTRICAL-AND-THERMOELECTRIC PROPERTIES

Here, if denoting, for majority electrons (holes), the electrical conductivity by $\sigma(N, r_{d(a)}, x, T)$, expressed in $\text{ohm}^{-1} \times \text{cm}^{-1}$, the thermal conductivity by $\kappa(N, r_{d(a)}, x, T)$, expressed in $\frac{\text{W}}{\text{cm} \times \text{K}}$, and Lorenz number L by:

$L = \frac{\pi^2}{3} \times \left(\frac{k_B}{q}\right)^2 = 2.4429637 \left(\frac{\text{W} \times \text{ohm}}{\text{K}^2}\right) = 2.4429637 \times 10^{-8} (\text{V}^2 \times \text{K}^{-2})$, then the well-known Wiedemann-Frank law states that the ratio, $\frac{\kappa}{\sigma}$, is proportional to the temperature $T(\text{K})$, as:

$$\frac{\kappa(N, r_{d(a)}, x, T)}{\sigma(N, r_{d(a)}, x, T)} = L \times T. \tag{13}$$

We now determine the general form of σ in the following.

First, it is expressed in terms of the kinetic energy of the electron (hole), $E_k \equiv \frac{\hbar^2 \times k^2}{2 \times m_{Cn(Cp)} \times m_0}$, or the wave number k , as:

$$\sigma(k) \equiv \frac{q^2 \times k}{\pi \times \hbar} \times \frac{k}{k_{sn(sp)}} \times [k \times a_{Bn(Bp)}] \times \left(\frac{E_k}{\eta_{n(p)}}\right)^{1/2},$$

which is thus proportional to E_k^2 .

Then, for $E \geq 0$, we obtain: $\langle E^2 \rangle_{FDDF} \equiv G_2(y = \frac{\pi k_B T}{E_{Fn(Fp)}}) \times E_{Fn(Fp)}^2$, and $G_2(y) = \left(1 + \frac{y^2}{3}\right) \equiv G_2(N, r_{d(a)}, x, T)$, with $y \equiv \frac{\pi}{\xi_{n(p)}}$, $\xi_{n(p)} = \xi_{n(p)}(N, r_{d(a)}, x, T)$ for a presentation simplicity. Therefore, one obtains:

$$\sigma(N, r_{d(a)}, x, T) \equiv \left[\frac{q^2}{\pi \times \hbar} \times \frac{k_{Fn(Fp)}(N^*)}{R_{sn(sp)}(N^*)} \times [k_{Fn(Fp)}(N^*) \times a_{Bn(Bp)}(r_{d(a)})] \times \sqrt{A_{n(p)}(N^*)} \right] \times \left[G_2(N, r_{d(a)}, x, T) \times \left(\frac{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}{E_{Fno(Fpo)}(N^*)}\right)^2 \right] \left(\frac{1}{\text{ohm} \times \text{cm}}\right),$$

$$\frac{q^2}{\pi \times \hbar} = 7.7480735 \times 10^{-5} \text{ ohm}^{-1}, A_{n(p)}(N^*) = \frac{E_{Fno(Fpo)}(N^*)}{\eta_{n(p)}(N^*)}, \tag{14}$$

which also determine the resistivity as: $\rho(N, r_{d(a)}, x, T) \equiv 1/\sigma(N, r_{d(a)}, x, T)$, noting that $N^* \equiv N - N_{CDn(NDp)}(r_{d(a)}, x)$. **This $\sigma(N, r_{d(a)}, x, T)$ -result is an essential one in this paper.**

In Eq. (14), one notes that at $T=0\text{ K}$, $\sigma(N, r_{d(a)}, x, T = 0\text{K})$ is proportional to $E_{Fno(Fpo)}^{\frac{3}{2}}$, or to N^* . Thus, $\sigma(N = N_{CDn(NDp)}, r_{d(a)}, x, T = 0\text{K}) = 0$ at $N^* = 0$, at which the metal-insulator transition (MIT) occurs.

Electrical Coefficients

The relaxation time τ is related to σ by:

$$\tau(N, r_{d(a)}, x, T) \equiv \sigma(N, r_{d(a)}, x, T) \times \frac{m_{c(v)}(x) \times m_0}{q^2 \times N^*}. \text{ Therefore, the mobility } \mu \text{ is given by:}$$

$$\mu(N, r_{d(a)}, x, T) \equiv \mu(N^*, r_{d(a)}, T) = \frac{q \times \tau(N, r_{d(a)}, x, T)}{m_{c(v)}(x) \times m_0} = \frac{\sigma(N, r_{d(a)}, x, T)}{q \times N^*} \left(\frac{\text{cm}^2}{\text{V} \times \text{s}} \right). \tag{15}$$

Here, at $T=0\text{K}$, $\mu(N^*, r_{d(a)}, T)$ is thus proportional to $(N^*)^{1/3}$, since $\sigma(N^*, r_{d(a)}, T = 0\text{K})$ is proportional to $(N^*)^{4/3}$. Thus, $\mu(N^* = 0, r_{d(a)}, T = 0\text{K}) = 0$ at $N^* = 0$, at which the metal-insulator transition (MIT) occurs.

Then, since τ and σ are both proportional to $E_{Fn(Fp)}(N^*, T)^2$, as given above, the Hall factor can thus be determined by:

$$r_H(N, r_{d(a)}, x, T) \equiv \frac{(\tau^2)_{FDDF}}{[(\tau)_{FDDF}]^2} = \frac{G_4(y)}{[G_2(y)]^2}, y \equiv \frac{\pi}{\xi_{n(p)}(N, r_{d(a)}, x, T)} = \frac{\pi k_B T}{E_{Fn(Fp)}(N, r_{d(a)}, x, T)}, \text{ and therefore,}$$

the Hall mobility yields:

$$\mu_H(N, r_{d(a)}, x, T) \equiv \mu(N, r_{d(a)}, x, T) \times r_H(N^*, T) \left(\frac{\text{cm}^2}{\text{V} \times \text{s}} \right), \tag{16}$$

noting that, at $T=0\text{K}$, since $r_H(N, r_{d(a)}, x, T) = 1$, one then gets at $N = N_{CDn(NDp)}$:

$$\mu_H(N, r_{d(a)}, x, T) \equiv \mu(N, r_{d(a)}, x, T) = 0 \text{ at } N^* = 0, \text{ at which the metal-insulator transition (MIT) occurs.}$$

Finally, the **generalized Einstein relation** is found to be defined (Van Cong, 1980) as:

$$\frac{D(N, r_{d(a)}, x, T)}{\mu(N, r_{d(a)}, x, T)} \equiv \frac{N}{q} \times \frac{dE_{Fn(Fp)}}{dN} \equiv \frac{k_B \times T}{q} \times \left(u \frac{d\xi_{n(p)}(u)}{du} \right),$$

where $D(N^*, r_{d(a)}, T)$ is the diffusion coefficient, $\xi_{n(p)}(u)$ is defined in Eq. (11), and the mobility $\mu(N, r_{d(a)}, x, T)$ is determined in Eq. (15). Then, by differentiating this function $\xi_{n(p)}(u)$ with respect to u , one thus obtains $\frac{d\xi_{n(p)}(u)}{du}$. Therefore,

$$\frac{D(N^*, r_{d(a)}, T)}{\mu(N^*, r_{d(a)}, T)} = \frac{k_B \times T}{q} \times u \frac{V'(u) \times W(u) - V(u) \times W'(u)}{W^2(u)}, \tag{17}$$

where $W'(u) = ABu^{B-1}$ and

$$V'(u) = u^{-1} + 2^{-\frac{3}{2}} e^{-du} (1 - du) + \frac{2}{3} Au^{B-1} F(u) \left[\left(1 + \frac{3B}{2}\right) + \frac{4}{3} \times \frac{bu^{-\frac{4}{3}} + 2cu^{-\frac{8}{3}}}{1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}}} \right].$$

One remarks that: (i) as $u \rightarrow 0$, one has: $W^2 \simeq 1$ and $u[V' \times W - V \times W'] \simeq 1$, and therefore:

$$\frac{D_{n(p)}(u)}{\mu} \simeq \frac{k_B \times T}{q}, \quad \text{and} \quad \text{(ii) as } u \rightarrow \infty, \quad \text{one has: } W^2 \approx A^2 u^{2B} \quad \text{and}$$

$u[V' \times W - V \times W'] \approx \frac{2}{3} au^{2/3} A^2 u^{2B}$, and therefore, in this **highly degenerate case** and at

$T=0K$, the **above generalized Einstein relation** is reduced to the **usual Einstein one**:

$$\frac{D(N^*, r_{d(a)}, T=0)}{\mu(N^*, r_{d(a)}, T=0)} \approx \frac{2}{3} E_{Fno(Fpo)}(N^*)/q. \quad \text{In other words, Eq. (17) verifies the correct limiting$$

conditions.

One also notes that, for $N^* = 0$, $\mu(N^* = 0, r_{d(a)}, T = 0K) = 0$, as remarked in above, and therefore, for any $r_{d(a)}$, $D(N^* = 0, r_{d(a)}, T = 0K) = 0$, according to the MIT.

Further, in the present degenerate case ($u \gg 1$), Eq. (17) gives:

$$\frac{D(N, r_{d(a)}, x, T)}{\mu(N, r_{d(a)}, x, T)} \simeq \frac{2}{3} \times \frac{E_{Fno(Fpo)}(u)}{q} \times \left[1 + \frac{4}{3} \times \frac{\left(bu^{-\frac{4}{3}} + 2cu^{-\frac{8}{3}}\right)}{\left(1 + bu^{-\frac{4}{3}} + cu^{-\frac{8}{3}}\right)} \right], \quad (18)$$

where $a = [(3\sqrt{\pi}/4)]^{2/3}$, $b = \frac{1}{8} \left(\frac{\pi}{a}\right)^2$ and $c = \frac{62.3739855}{1920} \left(\frac{\pi}{a}\right)^4$.

In **Tables 3n(3p) given in Appendix 1**, for given x , N and $T(=4.2 K$ and $77 K)$, and from Equations (14, 15, 16, 18), the numerical results of the coefficients: σ, μ, μ_H, D , expressed respectively in $\left(\frac{10^8}{ohm \times cm}, \frac{10^8 \times cm^2}{V \times s}, \frac{10^8 \times cm^2}{V \times s}, \frac{10 \times cm^2}{s}\right)$, are found to be decreased with increasing $r_{d(a)}$, respectively.

Thermoelectric Coefficients

First off all, from Eq. (14), obtained for $\sigma(N, r_{d(a)}, x, T)$, the well-known Mott definition for the thermoelectric power or for the Seebeck coefficient, S , is given by:

$$S(N, r_{d(a)}, x, T) \equiv \frac{-\pi^2}{3} \times \frac{k_B}{q_{>0}} \times k_B T \times \left. \frac{\partial \ln \sigma(E)}{\partial E} \right]_{E=E_{Fn(Fp)}} = \frac{-\pi^2}{3} \times \frac{k_B}{q} \times \frac{\partial \ln \sigma(\xi_{n(p)})}{\partial \xi_{n(p)}}.$$

Then, using Eq. (11), for $\xi_{n(p)}(N, r_{d(a)}, x, T) \gtrsim 1$, one gets, by putting

$$F_S(N, r_{d(a)}, x, T) \equiv \left[1 - \frac{y^2}{3 \times G_2 \left(y = \frac{\pi}{\xi_{n(p)}} \right)} \right],$$

$$S(N, r_{d(a)}, x, T) \equiv \frac{-\pi^2}{3} \times \frac{k_B}{q} \times \frac{2F_{Sb}(N^*, T)}{\xi_{n(p)}} = -\sqrt{\frac{3 \times L}{\pi^2}} \times \frac{2 \times \xi_{n(p)}}{\left(1 + \frac{3 \times \xi_{n(p)}^2}{\pi^2} \right)} \left(\frac{V}{K} \right), \quad (19)$$

giving here: (i) at $\xi_{n(p)} = \sqrt{\frac{\pi^2}{3}} \simeq 1.8138$, one gets: $S = -\sqrt{L} \simeq -1.563 \times 10^{-4} \left(\frac{V}{K} \right)$ and at $\xi_{n(p)} = 1$ one obtains: $S \simeq -1.322 \times 10^{-4} \left(\frac{V}{K} \right)$.

Further, the figure of merit, ZT, is found to be given by:

$$ZT(N, r_{d(a)}, x, T) \equiv \frac{S^2 \times \sigma \times T}{\kappa} = \frac{S^2}{L} = (ZT)_{Mott} \times [2 \times F_S]^2, \quad (ZT)_{Mott} = \frac{\pi^2}{3 \times \xi_{n(p)}^2}, \quad (20)$$

giving here: (i) at $\xi_{n(p)} = \sqrt{\frac{\pi^2}{3}} \simeq 1.8138$, one gets: $ZT = (ZT)_{Mott} = 1$, and at $\xi_{n(p)} = 1$ one obtains: $ZT \simeq 0.715$ and $(ZT)_{Mott} = \frac{\pi^2}{3} \simeq 3.290$.

Furthermore, from Eq. (19), one gets:

$$\frac{\partial S}{\partial \xi_{n(p)}} = \sqrt{\frac{3 \times L}{\pi^2}} \times \frac{\frac{3 \times \xi_{n(p)}^2}{\pi^2} - 1}{\left(1 + \frac{3 \times \xi_{n(p)}^2}{\pi^2} \right)^2}, \quad \frac{dS}{dT} = \frac{\partial S}{\partial \xi_{n(p)}} \times \frac{\partial \xi_{n(p)}}{\partial T}, \quad \text{and} \quad \frac{dS}{dN} = \frac{\partial S}{\partial \xi_{n(p)}} \times \frac{\partial \xi_{n(p)}}{\partial N}, \quad \text{and}$$

$$\frac{d(ZT)}{dT} = \frac{2 \times S}{L} \times \frac{dS}{dT} \quad \text{and} \quad \frac{d(ZT)}{dN} = \frac{2 \times S}{L} \times \frac{dS}{dN}, \quad (21)$$

noting that: (i) at given $(N, r_{d(a)}, x)$, and for $\frac{\partial \xi_{n(p)}}{\partial T} > 0$ (or < 0), $\xi_{n(p)}$ increases (or decreases) for decreasing (or increasing) T, (ii) at given $(r_{d(a)}, x, T)$, and for $\frac{\partial \xi_{n(p)}}{\partial N} > 0$ (or < 0), $\xi_{n(p)}$ increases (or decreases) for increasing (or decreasing) N.

Finally, the Van-Cong coefficient, VC, is given by:

$$VC(N, r_{d(a)}, x, T) \equiv N \times \frac{dS}{dN} \left(\frac{V}{K} \right), \quad (22)$$

the Thomson coefficient, Ts, by:

$$Ts(N, r_{d(a)}, x, T) \equiv T \times \frac{dS}{dT} \left(\frac{V}{K} \right), \quad (23)$$

and then, the Peltier coefficient, P_t , as:

$$P_t(N, r_{d(a)}, x, T) \equiv T \times S \text{ (V)}. \quad (24)$$

Now, in the lightly degenerate n(p)-type $\text{InSb}_{1-x}\text{As}_x$ alloy, in which $N=5 \times 10^{17} \text{ cm}^{-3}$ ($5 \times 10^{18} \text{ cm}^{-3}$), and for $T=3\text{K}$ and 80K , the numerical results of various thermoelectric coefficients are reported in Tables 4n(4p) in Appendix 1, noting that their variations with increasing $r_{d(a)}$ are represented by the arrows: ↗ (increase), and ↘ (decrease), respectively.

Then, in Tables 5n(5p) given Appendix 1 for a given N and with increasing T , and then in Tables 6n(6p) given Appendix 1 for a given T and with decreasing N , the reduced Fermi-energy $\xi_{n(p)}$ decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘).

One notes here that with increasing T (or with decreasing N) one obtains: (i) for $\xi_{n(p)} \simeq 1.8138$, while the numerical results of S present a same minimum $(S)_{\min.} \left(\simeq -1.563 \times 10^{-4} \frac{\text{V}}{\text{K}} \right)$, those of ZT show a same maximum $(ZT)_{\max.} = 1$, (ii) for $\xi_{n(p)} = 1$, those of S , ZT , $(ZT)_{\text{Mott}}$, VC , and T_s present the same results: $-1.322 \times 10^{-4} \frac{\text{V}}{\text{K}}$, 0.715 , 3.290 , $-1.105 \times 10^{-4} \frac{\text{V}}{\text{K}}$, and $1.657 \times 10^{-4} \frac{\text{V}}{\text{K}}$, respectively, and (iii) for $\xi_n \simeq 1.8138$, $(ZT)_{\text{Mott}} = 1$. It seems that these results could present a new law in the thermoelectric properties, obtained in the degenerate case.

CONCLUDING REMARKS

In the $n^+(p^+) - p(n)$ $\text{InSb}_{1-x}\text{As}_x$ - crystalline alloy, all the numerical results of electrical-and-thermoelectric coefficients, obtained in our previous work (Van Cong, 2018), were revised and performed, by basing on our following basic expressions.

(1) The effective extrinsic static dielectric constant law, $\varepsilon(r_{d(a)}, x)$, due to the impurity size effect, is determined in Eq. (1).

(2) The generalized Mott criterium in the metal-insulator transition is expressed in Equations (3, 5, 6), showing that $N_{\text{CDn(CDp)}}$ is just the density of electrons (holes) localized in the exponential conduction (valence)-band tail, $N_{\text{CDn(CDp)}}^{\text{EBT}}$, with a precision of the order of 2.86×10^{-7} , as given in our recent work (Van Cong, 2024), and the effective electron

(hole)-density: $N^* \equiv N - N_{CDn(CDp)} \simeq N - N_{CDn(CDp)}^{EBT}$, as that observed in the compensated crystals.

(3) The ratio of the inverse effective screening length $k_{sn(sp)}$ to Fermi wave number $k_{Fn(kp)}$ at 0 K, $R_{sn(sp)}(N^*)$, defined in Eq. (7), is valid at any density N^* .

(4) The Fermi energy for any N and T , $E_{Fn(Fp)}$, determined in Eq. (11) with a precision of the order of 2.11×10^{-4} (Van Cong, 1993), and it exists in all the expressions of electrical-and-thermoelectric coefficients.

(5) Our expressions for the electrical conductivity, σ , and for the Seebeck coefficient, S , determined respectively in Equations (14, 19) are the basic expressions for determining the electrical-and-thermoelectric coefficients.

(6) Finally, in Tables 5n(5p) given Appendix 1 for a given N and with increasing T , and then in Tables 6n(6p) given Appendix 1 for a given T and with decreasing N , the reduced Fermi-energy $\xi_{n(p)}$ decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T (or with decreasing N) one obtains: (i) for $\xi_{n(p)} \simeq 1.8138$, while the numerical results of S present a **same minimum** $(S)_{min.} (\simeq -1.563 \times 10^{-4} \frac{V}{K})$, those of ZT show a **same maximum** $(ZT)_{max.} = 1$, (ii) for $\xi_{n(p)} = 1$, those of S , ZT , $(ZT)_{Mott}$, VC , and T_s present **the same results**: $-1.322 \times 10^{-4} \frac{V}{K}$, 0.715 , 3.290 , $-1.105 \times 10^{-4} \frac{V}{K}$, and $1.657 \times 10^{-4} \frac{V}{K}$, respectively, and (iii) for $\xi_n \simeq 1.8138$, $(ZT)_{Mott} = 1$. It seems that these results could present a new law in the thermoelectric properties, obtained in the degenerate case.

In summary, all the numerical results of electrical-and-thermoelectric coefficients, given in our previous work (Van Cong, 2018), are now revised and performed.

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APPENDIX 1

Table 1: The values of various energy-band-structure parameters are given in various crystalline alloys as follows.

In $InSb_{1-x}As_x$ -alloy, in which $r_{do(As)} = r_{Sb(M)} = 0.136$ nm (0.144 nm), we have: $g_{c(v)}(x) = 1 \times x + 1 \times (1 - x)$, $m_{c(v)}(x)/m_0 = 0.09 (0.3) \times x + 0.1 (0.4) \times (1 - x)$, $\epsilon_0(x) = 14.55 \times x + 16.9 \times (1 - x)$, $E_{go}(x) = 0.43 \times x + 0.23 \times (1 - x)$.

Table 2: Expressions for $G_{p \geq 1}(y \equiv \frac{\pi}{\xi_{n(p)}})$, due to the Fermi-Dirac distribution function, noting that $G_{p=1}(y \equiv \frac{\pi k_B T}{E_{Fn(Fp)}} = \frac{\pi}{\xi_{n(p)}}) = 1$, used to determine the electrical-and-thermoelectric coefficients.

$G_{3/2}(y)$	$G_2(y)$	$G_{5/2}(y)$	$G_3(y)$	$G_{7/2}(y)$	$G_4(y)$	$G_{9/2}(y)$
$(1 + \frac{y^2}{8} + \frac{7y^4}{640})$	$(1 + \frac{y^2}{3})$	$(1 + \frac{5y^2}{8} - \frac{7y^4}{384})$	$(1 + y^2)$	$(1 + \frac{35y^2}{24} + \frac{49y^4}{384})$	$(1 + 2y^2 + \frac{7y^4}{15})$	$(1 + \frac{21y^2}{8} + \frac{147y^4}{128})$

Table 3n: Here, one notes that, for given x, N and T(=4.2 K and 77 K), the functions: σ, μ, μ_H, D , expressed respectively in $(\frac{10^3}{ohm \times cm}, \frac{10^3 \times cm^2}{V \times s}, \frac{10^3 \times cm^2}{V \times s}, \frac{10^2 \times cm^2}{s})$, decrease with increasing r_d .

Donor	P	As	Sb	Sn
r_d (nm)	↗ 0.110	0.118	0.136	0.140

For x=0, the values of (σ, μ, μ_H, D) at 4.2K

N (10^{18} cm^{-3})

3	1.69, 3.525, 3.526, 1.78	1.48, 3.098, 3.099, 1.56	1.33, 2.793, 2.794, 1.40	1.32, 2.779, 2.780, 1.40
10	4.39, 2.745, 2.746, 3.09	3.82, 2.387, 2.388, 2.69	3.41, 2.136, 2.136, 2.41	3.40, 2.124, 2.124, 2.39
40	14.0, 2.185, 2.185, 6.21	12.0, 1.874, 1.874, 5.33	10.6, 1.658, 1.658, 4.71	10.5, 1.648, 1.648, 4.68
70	22.7, 2.026, 2.026, 8.36	19.4, 1.730, 1.730, 7.14	17.1, 1.524, 1.524, 6.29	17.0, 1.515, 1.515, 6.25

For x=0.5, the values of (σ, μ, μ_H, D) at 4.2K

N (10^{18} cm^{-3})

3	1.76, 3.686, 3.687, 1.95	1.54, 3.236, 2.237, 1.71	1.39, 2.915, 2.916, 1.54	1.38, 2.900, 2.901, 1.53
10	4.63, 2.891, 2.891, 3.43	4.01, 2.509, 2.510, 2.98	3.58, 2.241, 2.242, 2.66	3.56, 2.230, 2.230, 2.64
40	14.9, 2.321, 2.321, 6.94	12.7, 1.988, 1.988, 5.95	11.2, 1.756, 1.756, 5.25	11.1, 1.745, 1.745, 5.22
70	24.2, 2.159, 2.159, 9.38	20.6, 1.841, 1.841, 8.00	18.1, 1.620, 1.620, 7.04	18.0, 1.609, 1.609, 6.99

For x=1, the values of (σ, μ, μ_H, D) at 4.2K

N (10^{18} cm^{-3})

3	1.87, 3.905, 3.906, 2.19	1.63, 3.421, 3.422, 1.91	1.47, 3.078, 3.079, 1.72	1.46, 3.062, 3.063, 1.71
10	4.95, 3.091, 3.092, 3.87	4.28, 2.677, 2.677, 3.35	3.81, 2.386, 2.387, 2.99	3.79, 2.373, 2.374, 2.97
40	16.1, 2.508, 2.508, 7.92	13.7, 2.144, 2.144, 6.77	12.1, 1.890, 1.890, 5.97	12.0, 1.879, 1.879, 5.93
70	26.2, 2.341, 2.341, 10.7	22.3, 1.992, 1.992, 9.14	19.6, 1.750, 1.750, 8.03	19.5, 1.739, 1.739, 7.97

For $x=0$, the values of (σ, μ, μ_H, D) at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.74, 3.630, 3.930, 1.85	1.52, 3.191, 3.499, 1.62	1.37, 2.877, 3.155, 1.46	1.36, 2.862, 3.139, 1.45
10	4.42, 2.762, 2.817, 3.12	3.84, 2.402, 2.450, 2.71	3.43, 2.149, 2.192, 2.42	3.42, 2.137, 2.180, 2.41
40	14.0, 2.187, 2.194, 6.22	12.0, 1.876, 1.882, 5.33	10.6, 1.660, 1.665, 4.72	10.6, 1.650, 1.655, 4.69
70	22.7, 2.027, 2.030, 8.37	19.4, 1.731, 1.734, 7.15	17.1, 1.525, 1.527, 6.29	17.0, 1.516, 1.518, 6.26

For $x=0.5$, the values of (σ, μ, μ_H, D) at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.81, 3.785, 4.116, 2.02	1.59, 3.323, 3.614, 1.78	1.43, 2.993, 3.256, 1.60	1.42, 2.978, 3.240, 1.59
10	4.65, 2.907, 2.960, 3.45	4.03, 2.523, 2.569, 3.00	3.60, 2.254, 2.295, 2.68	3.58, 2.242, 2.282, 2.66
40	14.9, 2.323, 2.329, 6.95	12.7, 1.990, 1.995, 5.95	11.2, 1.757, 1.763, 5.26	11.2, 1.747, 1.752, 5.23
70	24.2, 2.160, 2.163, 9.39	20.6, 1.842, 1.844, 8.00	18.2, 1.620, 1.622, 7.04	18.0, 1.610, 1.612, 7.00

For $x=1$, the values of (σ, μ, μ_H, D) at 77 K

$N (10^{18} \text{ cm}^{-3})$

3	1.91, 3.999, 4.315, 2.26	1.67, 3.504, 3.782, 1.97	1.50, 3.153, 3.403, 1.77	1.49, 3.137, 3.385, 1.76
10	4.97, 3.107, 3.157, 3.90	4.30, 2.690, 2.734, 3.37	3.83, 2.398, 2.438, 3.01	3.81, 2.385, 2.424, 2.99
40	16.1, 2.510, 2.516, 7.93	13.7, 2.145, 2.151, 6.77	12.1, 1.892, 1.896, 5.97	12.0, 1.880, 1.885, 5.94
70	26.3, 2.342, 2.345, 10.7	22.3, 1.993, 1.996, 9.14	19.6, 1.751, 1.753, 8.03	19.5, 1.740, 1.742, 7.98

Table 3p: Here, one notes that, for given x , N and $T(=4.2 \text{ K}$ and $77 \text{ K})$, the functions: σ, μ, μ_H, D , expressed respectively in $(\frac{10^8}{\text{ohm}\times\text{cm}}, \frac{10^8 \times \text{cm}^2}{\text{V}\times\text{s}}, \frac{10^8 \times \text{cm}^2}{\text{V}\times\text{s}}, \frac{10 \times \text{cm}^2}{\text{s}})$, decrease with increasing r_a .

Acceptor	Ga	Mg	In	Sn
r_a (nm)	↗ 0.120	0.140	0.144	0.148

For $x=0$, the values of (σ, μ, μ_H, D) at 4.2K

$N (10^{18} \text{ cm}^{-3})$

3	0.47, 1.598, 1.613, 1.47	0.37, 1.460, 1.477, 1.21	0.37, 1.454, 1.470, 1.20	0.36, 1.448, 1.464, 1.19
10	1.92, 1.356, 1.358, 3.53	1.67, 1.210, 1.211, 3.09	1.65, 1.203, 1.204, 3.06	1.64, 1.196, 1.197, 3.04
40	7.52, 1.209, 1.209, 8.43	6.63, 1.072, 1.072, 7.44	6.58, 1.065, 1.065, 7.39	6.54, 1.058, 1.059, 7.34
70	12.8, 1.164, 1.164, 11.9	11.3, 1.031, 1.031, 10.5	11.2, 1.024, 1.024, 10.4	11.2, 1.018, 1.018, 10.3

For $x=0.5$, the values of (σ, μ, μ_H, D) at 4.2K

 $N (10^{18} \text{ cm}^{-3})$

3	0.57, 1.732, 1.743, 1.94	0.46, 1.574, 1.585, 1.64	0.45, 1.566, 1.577, 1.63	0.45, 1.559, 1.570, 1.61
10	2.15, 1.484, 1.485, 4.48	1.87, 1.323, 1.325, 3.93	1.86, 1.316, 1.317, 3.90	1.85, 1.308, 1.309, 3.88
40	8.28, 1.324, 1.324, 10.6	7.30, 1.173, 1.173, 9.35	7.26, 1.166, 1.166, 9.29	7.21, 1.159, 1.159, 9.23
70	14.1, 1.275, 1.275, 14.9	12.4, 1.129, 1.129, 13.2	12.3, 1.122, 1.122, 13.1	12.2, 1.114, 1.114, 13.0

 For $x=1$, the values of (σ, μ, μ_H, D) at **4.2K**

 $N (10^{18} \text{ cm}^{-3})$

3	0.69, 1.924, 1.931, 2.68	0.58, 1.740, 1.747, 2.30	0.57, 1.731, 1.739, 2.29	0.57, 1.722, 1.730, 2.27
10	2.46, 1.661, 1.662, 5.93	2.16, 1.481, 1.482, 5.22	2.14, 1.472, 1.473, 5.19	2.13, 1.463, 1.464, 5.16
40	9.32, 1.482, 1.482, 13.9	8.23, 1.314, 1.314, 12.3	8.18, 1.306, 1.306, 12.2	8.12, 1.298, 1.298, 12.1
70	15.8, 1.427, 1.427, 19.5	14.0, 1.264, 1.264, 17.2	13.9, 1.256, 1.256, 17.1	13.8, 1.248, 1.248, 17.0

 For $x=0$, the values of (σ, μ, μ_H, D) at **77K**

 $N (10^{18} \text{ cm}^{-3})$

3	0.27, 0.909, 2.709, 0.65	0.18, 0.694, 2.251, 0.41	0.17, 0.682, 2.226, 0.40	0.16, 0.671, 2.199, 0.39
10	2.12, 1.498, 1.978, 4.04	1.85, 1.341, 1.785, 3.55	1.83, 1.333, 1.775, 3.53	1.82, 1.326, 1.766, 3.50
40	7.64, 1.228, 1.291, 8.60	6.73, 1.088, 1.145, 7.59	6.69, 1.082, 1.138, 7.54	6.64, 1.075, 1.131, 7.49
70	12.9, 1.173, 1.201, 12.0	11.4, 1.038, 1.064, 10.6	11.3, 1.032, 1.057, 10.5	11.2, 1.025, 1.051, 10.4

 For $x=0.5$, the values of (σ, μ, μ_H, D) at **77K**

 $N (10^{18} \text{ cm}^{-3})$

3	0.43, 1.318, 3.226, 1.31	0.32, 1.087, 2.865, 0.96	0.31, 1.075, 2.847, 0.95	0.31, 1.063, 2.828, 0.93
10	2.32, 1.603, 2.001, 4.97	2.03, 1.433, 1.798, 4.38	2.02, 1.425, 1.789, 4.35	2.00, 1.417, 1.779, 4.32
40	8.38, 1.339, 1.392, 10.7	7.39, 1.187, 1.235, 9.49	7.34, 1.180, 1.227, 9.43	7.29, 1.173, 1.220, 9.37
70	14.2, 1.282, 1.306, 15.0	12.5, 1.135, 1.156, 13.3	12.4, 1.128, 1.149, 13.2	12.3, 1.121, 1.142, 13.1

 For $x=1$, the values of (σ, μ, μ_H, D) at **77K**

 $N (10^{18} \text{ cm}^{-3})$

3	0.68, 1.883, 3.685, 2.60	0.54, 1.613, 3.325, 2.07	0.53, 1.600, 3.308, 2.04	0.52, 1.586, 3.290, 2.02
10	2.61, 1.758, 2.080, 6.40	2.28, 1.569, 1.863, 5.65	2.27, 1.560, 1.853, 5.61	2.25, 1.551, 1.843, 5.57
40	9.40, 1.495, 1.538, 14.0	8.30, 1.325, 1.364, 12.4	8.25, 1.317, 1.356, 12.3	8.20, 1.309, 1.347, 12.2
70	15.9, 1.433, 1.453, 19.6	14.0, 1.269, 1.286, 17.3	13.9, 1.261, 1.278, 17.2	13.8, 1.253, 1.270, 17.1

Table 4n. In the lightly degenerate n-type $\text{InSb}_{1-x}\text{As}_x$ alloy, in which $N=5 \times 10^{17} \text{ cm}^{-3}$, and for $T=3\text{K}$ and 80K , the numerical results of various thermoelectric coefficients are reported. Further, their variations with increasing $r_{d(a)}$ are represented by the arrows: ↗ (increase), and ↘ (decrease).

Donor		P	As	Sb	Sn
For x=0,					
$\xi_{n(T=3K)}$	↘	87.31	86.776	86.209	86.178
$\xi_{n(T=80K)}$	↘	3.30	3.270	3.240	3.238
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{\text{cm} \times K} \right)$	↘	3.076	2.678	2.383	2.369
$\kappa_{(T=80K)} \left(\frac{10^{-4} \times W}{\text{cm} \times K} \right)$	↘	8.330	7.213	6.380	6.340
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.491	6.531	6.574	6.576
$-S_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	13.201	13.260	13.324	13.327
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↗	4.322	4.349	4.377	4.379
$VC_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	6.477	6.472	6.463	6.4629
$-TS_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.484	6.523	6.566	6.568
$-TS_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↗	9.715	9.708	9.695	9.694
$-Pt_{(T=3K)}(10^{-5} \times V)$	↘	1.947	1.959	1.972	1.973
$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	1.056	1.061	1.066	1.0662
$ZT_{(T=3K)} (10^{-3})$	↗	1.725	1.746	1.769	1.770
$ZT_{(T=80K)}$	↗	0.713	0.7197	0.72665	0.72704
For x=0.5,					
$\xi_{n(T=3K)}$	↘	91.81	91.219	90.590	90.555
$\xi_{n(T=80K)}$	↘	3.53	3.497	3.466	3.464
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{\text{cm} \times K} \right)$	↘	3.209	2.797	2.492	2.478
$\kappa_{(T=80K)} \left(\frac{10^{-4} \times W}{\text{cm} \times K} \right)$	↘	9.054	7.855	6.960	6.918
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.173	6.213	6.256	6.259
$-S_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	12.714	12.776	12.843	12.846
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↗	4.111	4.138	4.166	4.168
$VC_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↗	6.402	6.422	6.440	6.4408
$-TS_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.167	6.206	6.249	6.252
$-TS_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	9.603	9.633	9.660	9.661
$-Pt_{(T=3K)}(10^{-5} \times V)$	↘	1.852	1.864	1.877	1.878
$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	1.017	1.022	1.0274	1.0277

$ZT_{(T=3K)} (10^{-3})$	↗	1.560	1.580	1.602	1.603
$ZT_{(T=80K)}$	↗	0.662	0.668	0.6751	0.6755
For x=1,					
$\xi_{n(T=3K)}$	↘	96.79	96.131	95.424	95.384
$\xi_{n(T=80K)}$	↘	3.77	3.738	3.704	3.702
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{cm \times K} \right)$	↘	3.382	2.951	2.632	2.617
$\kappa_{(T=80K)} \left(\frac{10^{-4} \times W}{cm \times K} \right)$	↘	9.869	8.580	7.619	7.574
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	5.856	5.896	5.940	5.942
$-S_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	12.214	12.278	12.347	12.351
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↗	3.900	3.927	3.956	3.957
$VC_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↗	6.161	6.224	6.244	6.246
$-TS_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	5.850	5.890	5.934	5.936
$-TS_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	9.241	9.298	9.356	9.359
$-Pt_{(T=3K)} (10^{-5} \times V)$	↘	1.757	1.769	1.7819	1.7826
$-Pt_{(T=80K)} (10^{-2} \times V)$	↘	0.977	0.982	0.9878	0.9881
$ZT_{(T=3K)} (10^{-3})$	↗	1.403	1.423	1.444	1.445
$ZT_{(T=80K)}$	↗	0.611	0.617	0.6240	0.6244

Table 4p. In the lightly degenerate p-type $InSb_{1-x}As_x$ alloy, in which $N=5 \times 10^{18} \text{ cm}^{-3}$, and for T=3K and 80K, the numerical results of various thermoelectric coefficients are reported. Further, their variations with increasing $r_{d(a)}$ are represented by the arrows: ↗ (increase), and ↘ (decrease).

Acceptor		Ga	Mg	In	Cd
For x=0,					
$\xi_{p(T=3K)}$	↘	86.689	82.794	82.571	82.341
$\xi_{p(T=80K)}$	↘	3.265	3.060	3.048	3.035
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{cm \times K} \right)$	↘	6.649	5.583	5.531	5.478
$\kappa_{(T=80K)} \left(\frac{10^{-3} \times W}{cm \times K} \right)$	↘	1.789	1.436	1.419	1.401
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.538	6.845	6.863	6.882
$-S_{(T=80K)} \left(\frac{10^{-4} \times V}{K} \right)$	↘	1.327	1.371	1.374	1.376
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↗	4.353	4.557	4.569	4.582
$VC_{(T=80K)} \left(\frac{10^{-5} \times V}{K} \right)$	↘	6.471	6.321	6.306	6.290
$-TS_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right)$	↘	6.530	6.836	6.854	6.873

$-Ts_{(T=30K)} \left(\frac{10^{-5} \times V}{K} \right) \nearrow$	9.707	9.482	9.459	9.435
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.961	2.053	2.059	2.065
$-Pt_{(T=30K)}(10^{-2} \times V) \searrow$	1.061	1.097	1.099	1.101
$ZT_{(T=3K)}(10^{-3}) \nearrow$	1.749	1.918	1.928	1.939
$ZT_{(T=30K)} \nearrow$	0.721	0.7696	0.772	0.775

For x=0.5,

$\xi_p(T=3K) \searrow$	102.48	98.88	98.67	98.46
$\xi_p(T=30K) \searrow$	4.029	3.866	3.857	3.847
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{cm \times K} \right) \searrow$	7.635	6.498	6.443	6.387
$\kappa_{(T=30K)} \left(\frac{10^{-3} \times W}{cm \times K} \right) \searrow$	2.285	1.917	1.899	1.880
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \searrow$	5.531	5.732	5.744	5.757
$-S_{(T=30K)} \left(\frac{10^{-4} \times V}{K} \right) \searrow$	1.170	1.202	1.204	1.206
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \nearrow$	3.684	3.818	3.826	3.834
$VC_{(T=30K)} \left(\frac{10^{-5} \times V}{K} \right) \nearrow$	5.815	6.037	6.049	6.062
$-Ts_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \searrow$	5.526	5.727	5.739	5.751
$-Ts_{(T=30K)} \left(\frac{10^{-5} \times V}{K} \right) \searrow$	8.723	9.055	9.074	9.093
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.659	1.720	1.723	1.727
$-Pt_{(T=30K)}(10^{-2} \times V) \searrow$	0.936	0.961	0.963	0.965
$ZT_{(T=3K)}(10^{-3}) \nearrow$	1.252	1.345	1.351	1.356
$ZT_{(T=30K)} \nearrow$	0.560	0.591	0.593	0.595

For x=1,

$\xi_p(T=3K) \searrow$	123.47	120.22	120.03	119.84
$\xi_p(T=30K) \searrow$	4.875	4.752	4.745	4.737
$\kappa_{(T=3K)} \left(\frac{10^{-5} \times W}{cm \times K} \right) \searrow$	8.950	7.711	7.651	7.590
$\kappa_{(T=30K)} \left(\frac{10^{-3} \times W}{cm \times K} \right) \searrow$	2.728	2.354	2.336	2.317
$-S_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \searrow$	4.591	4.715	4.722	4.730
$-S_{(T=30K)} \left(\frac{10^{-4} \times V}{K} \right) \searrow$	1.022	1.041	1.043	1.044
$VC_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \nearrow$	3.059	3.141	3.146	3.151
$VC_{(T=30K)} \left(\frac{10^{-5} \times V}{K} \right) \nearrow$	4.923	5.001	5.014	5.020
$-Ts_{(T=3K)} \left(\frac{10^{-6} \times V}{K} \right) \searrow$	4.588	4.712	4.719	4.727
$-Ts_{(T=30K)} \left(\frac{10^{-5} \times V}{K} \right) \searrow$	7.384	7.513	7.521	7.530
$-Pt_{(T=3K)}(10^{-5} \times V) \searrow$	1.377	1.414	1.417	1.419

$-Pt_{(T=80K)}(10^{-2} \times V)$	↘	0.817	0.833	0.834	0.835
$ZT_{(T=8K)}(10^{-3})$	↗	0.863	0.910	0.913	0.916
$ZT_{(T=80K)}$	↗	0.427	0.444	0.445	0.446

Table 5n: Here, for a given N and with increasing T , the reduced Fermi-energy ξ_n decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T : (i) for $\xi_n \approx 1.8138$, while the numerical results of S present a same minimum $(S)_{min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$, those of ZT show a same maximum $(ZT)_{max.} = 1$, (ii) for $\xi_n = 1$, those of S , ZT , $(ZT)_{Mott}$, VC , and T_s present the same results: $-1.322 \times 10^{-4} \frac{V}{K}$, 0.715, 3.290, $-1.105 \times 10^{-4} \frac{V}{K}$, and $1.657 \times 10^{-4} \frac{V}{K}$, respectively, and (iii) for $\xi_n \approx 1.8138$, $(ZT)_{Mott} = 1$.

For $x=0$,

In the degenerate P- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_P)$, one gets:

T(K)	↗	10	10.528	12	14.325731	14.5
ξ_n	↘	1.974	1.8138	1.442	1	0.972
$S(10^{-4} \frac{V}{K})$		-1.557	↘ -1.563 ↗	-1.523	↗ -1.322 ↗	-1.301
ZT		0.993	↗ 1 ↘	0.949	↘ 0.715 ↘	0.693
$(ZT)_{Mott}$	↗	0.844	1	1.581	3.290	3.484
$VC(10^{-4} \frac{V}{K})$		0.142	↘ -7.52×10^{-5} ↘	-0.423	↘ -1.105 ↘	-1.153
$T_s(10^{-4} \frac{V}{K})$		-0.213	↗ 1.13×10^{-4} ↗	0.635	↗ 1.657 ↗	1.730
$Pt(10^{-3}V)$		-1.557	↘ -1.645 ↘	-1.827	↘ -1.893 ↗	-1.887

In the degenerate As- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{As})$, one gets:

T(K)	↗	10	12.813	15	17.435302	17.5
ξ_n	↘	2.685	1.8138	1.372	1	0.991
$S(10^{-4} \frac{V}{K})$		-1.450	↘ -1.563 ↗	-1.504	↗ -1.322 ↗	-1.315
ZT		0.860	↗ 1 ↘	0.926	↘ 0.715 ↘	0.708
$(ZT)_{Mott}$	↗	0.456	1	1.748	3.290	3.348
$VC(10^{-4} \frac{V}{K})$		0.547	↘ -2.35×10^{-5} ↘	-0.519	↘ -1.105 ↘	-1.120
$T_s(10^{-4} \frac{V}{K})$		-0.820	↗ 3.53×10^{-5} ↗	0.779	↗ 1.657 ↗	1.680
$Pt(10^{-3}V)$		-1.450	↘ -2.003 ↘	-2.256	↘ -2.304 ↗	-2.302

In the degenerate Sb- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{Sb})$, one gets:

T(K)	↗	10	15.0335	16	20.4571662	20.5
ξ_n	↘	3.382	1.8138	1.631	1	0.995
$S(10^{-4} \frac{V}{K})$		-1.302	↘ -1.563 ↗	-1.554	↗ -1.322 ↗	-1.318
ZT		0.694	↗ 1 ↘	0.989	↘ 0.715 ↘	0.711
$(ZT)_{Mott}$	↗	0.287	1	1.236	3.290	3.322

$VC \left(10^{-4} \frac{V}{K}\right)$	0.647 ↘	0.21×10^{-5} ↘	-0.191 ↘	-1.105 ↘	-1.113
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.971 ↗	-3.22×10^{-5} ↗	0.286 ↗	1.657 ↗	1.670
$Pt (10^{-3}V)$	-1.302 ↘	-2.350 ↘	-2.487 ↘	-2.704 ↗	-2.702

In the degenerate Sn- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{Sn})$, one gets:

T(K)	↗	10	15.1525	16	20.6188	20.7
ξ_n	↘	3.418	1.8138	1.654	1	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.294 ↘	-1.563 ↗	-1.556 ↗	-1.322 ↗	-1.315	
ZT	0.686 ↗	1 ↘	0.991 ↘	0.715 ↘	0.708	
$(ZT)_{Mott}$	↗	0.281	1	1.203	3.290	3.351
$VC \left(10^{-4} \frac{V}{K}\right)$	0.646 ↘	-0.20×10^{-5} ↘	-0.165 ↘	-1.105 ↘	-1.121	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.969 ↗	3.08×10^{-5} ↗	0.248 ↗	1.657 ↗	1.681	
$Pt (10^{-3}V)$	-1.294 ↘	-2.368 ↘	-2.490 ↘	-2.725 ↗	-2.722	

For x=0.5,

In the degenerate P- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_p)$, one gets:

T(K)	↗	10	11.4883	12	15.6330543	15.7
ξ_n	↘	2.269	1.8138	1.685	1	0.990
$S \left(10^{-4} \frac{V}{K}\right)$	-1.524 ↘	-1.563 ↗	-1.559 ↗	-1.322 ↗	-1.314	
ZT	0.951 ↗	1 ↘	0.994 ↘	0.715 ↘	0.707	
$(ZT)_{Mott}$	↗	0.639	1	1.159	3.290	3.357
$VC \left(10^{-4} \frac{V}{K}\right)$	0.352 ↘	3.95×10^{-5} ↘	-0.131 ↘	-1.105 ↘	-1.122	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.528 ↗	-5.92×10^{-5} ↗	0.197 ↗	1.657 ↗	1.683	
$Pt (10^{-3}V)$	-1.524 ↘	-1.796 ↘	-1.870 ↘	-2.066 ↗	-2.064	

In the degenerate As- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{As})$, one gets:

T(K)	↗	10	13.9822	15	19.0263965	19.1
ξ_n	↘	3.056	1.8138	1.610	1	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.372 ↘	-1.563 ↗	-1.552 ↗	-1.322 ↗	-1.315	
ZT	0.770 ↗	1 ↘	0.986 ↘	0.715 ↘	0.708	
$(ZT)_{Mott}$	↗	0.352	1	1.271	3.290	3.350
$VC \left(10^{-4} \frac{V}{K}\right)$	0.632 ↘	-7.62×10^{-6} ↘	-0.216 ↘	-1.105 ↘	-1.120	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.948 ↗	1.14×10^{-5} ↗	0.325 ↗	1.657 ↗	1.681	
$Pt (10^{-3}V)$	-1.372 ↘	-2.185 ↘	-2.328 ↘	-2.515 ↗	-2.512	

In the degenerate Sb- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{Sb})$, one gets:

T(K)	↗	10	16.4055	17	22.324027	22.4
ξ_n	↘	3.782	1.8138	1.708	1	0.992

$S \left(10^{-4} \frac{V}{K}\right)$	-1.219 ↘	-1.563 ↗	-1.560 ↗	-1.322 ↗	-1.316
ZT	0.608 ↗	1 ↘	0.996 ↘	0.715 ↘	0.709
$(ZT)_{Mott}$ ↗	0.230	1	1.128	3.290	3.343
$VC \left(10^{-4} \frac{V}{K}\right)$	0.614 ↘	6.02×10^{-6} ↘	-0.106 ↘	-1.105 ↘	-1.118
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.922 ↗	-9.03×10^{-6} ↗	0.160 ↗	1.657 ↗	1.678
Pt ($10^{-3}V$)	-1.219 ↘	-2.564 ↘	-2.652 ↘	-2.950 ↗	-2.948

In the degenerate Sn- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{Sn})$, one gets:

T(K)	↗	10	16.535	17	22.500411	22.6
ξ_n	↘	3.818	1.8138	1.731	1	0.990
$S \left(10^{-4} \frac{V}{K}\right)$	-1.212 ↘	-1.563 ↗	-1.561 ↗	-1.322 ↗	-1.314	
ZT	0.601 ↗	1 ↘	0.998 ↘	0.715 ↘	0.707	
$(ZT)_{Mott}$ ↗	0.226	1	1.098	3.290	3.359	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.610 ↘	2.73×10^{-5} ↘	-0.082 ↘	-1.105 ↘	-1.123	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.915 ↗	-4.09×10^{-5} ↗	0.124 ↗	1.657 ↗	1.684	
Pt ($10^{-3}V$)	-1.212 ↘	-2.584 ↘	-2.654 ↘	-2.974 ↗	-2.970	

For x=1,

In the degenerate P- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_P)$, one gets:

T(K)	↗	10	12.633	12.7	17.18905	17.2
ξ_n	↘	2.628	1.8138	1.797	1	0.998
$S \left(10^{-4} \frac{V}{K}\right)$	-1.461 ↘	-1.563 ↗	-1.563 ↗	-1.322 ↗	-1.321	
ZT	0.874 ↗	1 ↘	0.999 ↘	0.715 ↘	0.714	
$(ZT)_{Mott}$ ↗	0.476	1	1.018	3.290	3.300	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.526 ↘	-2.46×10^{-4} ↘	-0.016 ↘	-1.105 ↘	-1.107	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.789 ↗	3.69×10^{-4} ↗	0.023 ↗	1.657 ↗	1.661	
Pt ($10^{-3}V$)	-1.461 ↘	-1.974 ↘	-1.985 ↘	-2.272 ↗	-2.271	

In the degenerate As- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDn}(r_{As})$, one gets:

T(K)	↗	10	15.375	16	20.920139	21
ξ_n	↘	3.484	1.8138	1.695	1	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	-1.280 ↘	-1.563 ↗	-1.559 ↗	-1.322 ↗	-1.315	
ZT	0.671 ↗	1 ↘	0.995 ↘	0.715 ↘	0.708	
$(ZT)_{Mott}$ ↗	0.271	1	1.144	3.290	3.349	
$VC \left(10^{-4} \frac{V}{K}\right)$	0.643 ↘	-2.19×10^{-4} ↘	-0.120 ↘	-1.105 ↘	-1.120	
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.964 ↗	3.3×10^{-4} ↗	0.180 ↗	1.657 ↗	1.680	
Pt ($10^{-3}V$)	-1.280 ↘	-2.403 ↘	-2.495 ↘	-2.765 ↗	-2.762	

In the degenerate Sb- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $N = 2 \times N_{\text{CDn}}(r_{\text{Sb}})$, one gets:

T(K)	↗	10	18.04	18.5	24.54599	24.6
ξ_n	↘	4.212	1.8138	1.738	1	0.995
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.135	-1.563	↗ -1.561	↗ -1.322	↗ -1.318
ZT		0.528	1	↘ 0.998	↘ 0.715	↘ 0.711
$(ZT)_{\text{Mott}}$	↗	0.185	1	1.089	3.290	3.324
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.557	-2.55×10^{-4}	↘ -0.075	↘ -1.105	↘ -1.114
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.835	3.82×10^{-4}	↗ 0.112	↗ 1.657	↗ 1.671
Pt (10^{-3}V)		-1.135	↘ -2.820	↘ -2.889	↘ -3.244	↗ -3.242

In the degenerate Sn- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $N = 2 \times N_{\text{CDn}}(r_{\text{Sn}})$, one gets:

T(K)	↗	10	18.1809	19	24.73993	24.8
ξ_n	↘	4.248	1.8138	1.683	1	0.994
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.129	-1.563	↗ -1.559	↗ -1.322	↗ -1.318
ZT		0.522	1	↘ 0.994	↘ 0.715	↘ 0.711
$(ZT)_{\text{Mott}}$	↗	0.182	1	1.161	3.290	3.328
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.552	6.15×10^{-6}	↘ -0.133	↘ -1.105	↘ -1.115
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.828	-9.23×10^{-6}	↗ 0.199	↗ 1.657	↗ 1.672
Pt (10^{-3}V)		-1.129	↘ -2.842	↘ -2.961	↘ -3.270	↗ -3.268

Table 5p: Here, for a given N and with increasing T , the reduced Fermi-energy ξ_p decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T : (i) for $\xi_p \approx 1.8138$, while the numerical results of S present a same minimum $(S)_{\text{min.}} (\approx -1.563 \times 10^{-4} \frac{\text{V}}{\text{K}})$, those of ZT show a same maximum $(ZT)_{\text{max.}} = 1$, (ii) for $\xi_p = 1$, those of S , ZT , $(ZT)_{\text{Mott}}$, VC , and T_s present the same results: $-1.322 \times 10^{-4} \frac{\text{V}}{\text{K}}$, 0.715 , 3.290 , $-1.105 \times 10^{-4} \frac{\text{V}}{\text{K}}$, and $1.657 \times 10^{-4} \frac{\text{V}}{\text{K}}$, respectively, and (iii) for $\xi_p \approx 1.8138$, $(ZT)_{\text{Mott}} = 1$.

For $x=0$,

In the degenerate Ga- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $N = 2 \times N_{\text{CDp}}(r_{\text{Ga}})$, one gets:

T(K)	↗	30	52.184	55	71.008677	71.5
ξ_p	↘	4.048	1.8138	1.659	1	0.984
$S \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-1.166	-1.563	↗ -1.557	↗ -1.322	↗ -1.310
ZT		0.557	1	↘ 0.992	↘ 0.715	↘ 0.703
$(ZT)_{\text{Mott}}$	↗	0.201	1	1.195	3.290	3.399
$VC \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		0.579	-5.42×10^{-5}	↘ -0.160	↘ -1.105	↘ -1.132
$T_s \left(10^{-4} \frac{\text{V}}{\text{K}}\right)$		-0.868	8.13×10^{-5}	↗ 0.239	↗ 1.657	↗ 1.699

Pt ($10^{-2}V$) -3.499 ↘ -8.156 ↘ -8.562 ↘ -9.385 ↗ -9.367

In the degenerate Mg- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(\Gamma_{Mg})$, one gets:

T(K)	↗	30	59.722	70	81.26823	81.3
ξ_p	↘	4.658	1.8138	1.369	1	0.999
$S \left(10^{-4} \frac{V}{K}\right)$		-1.057	-1.563	↗ -1.503	↗ -1.322	↗ -1.321
ZT		0.457	1	↘ 0.925	↘ 0.715	↘ 0.714
$(ZT)_{Mott}$	↗	0.152	1	1.756	3.290	3.296
$VC \left(10^{-4} \frac{V}{K}\right)$		0.508	↘ 2.86×10^{-5}	↘ -0.524	↘ -1.105	↘ -1.106
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.762	↗ -4.30×10^{-5}	↗ 0.786	↗ 1.657	↗ 1.660
Pt ($10^{-2}V$)		-0.317	↘ -0.934	↘ -1.052	↘ -1.07412	↗ -1.07402

In the degenerate In- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(\Gamma_{In})$, one gets:

T(K)	↗	30	60.135	70	81.828665	81.9
ξ_p	↘	4.689	1.8138	1.387	1	0.998
$S \left(10^{-4} \frac{V}{K}\right)$		-1.052	-1.563	↗ -1.508	↗ -1.322	↗ -1.320
ZT		0.453	1	↘ 0.931	↘ 0.715	↘ 0.713
$(ZT)_{Mott}$	↗	0.150	1	1.710	3.290	3.303
$VC \left(10^{-4} \frac{V}{K}\right)$		0.506	↘ -2.68×10^{-5}	↘ -0.499	↘ -1.105	↘ -1.108
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.759	↗ 4.02×10^{-5}	↗ 0.748	↗ 1.657	↗ 1.663
Pt ($10^{-2}V$)		-0.315	↘ -0.940	↘ -1.056	↘ -1.08153	↗ -1.08129

In the degenerate Cd- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(\Gamma_{Cd})$, one gets:

T(K)	↗	30	60.558	70	82.404885	82.5
ξ_p	↘	4.721	1.8138	1.405	1	0.997
$S \left(10^{-4} \frac{V}{K}\right)$		-1.046	-1.563	↗ -1.513	↗ -1.322	↗ -1.320
ZT		0.448	1	↘ 0.938	↘ 0.715	↘ 0.713
$(ZT)_{Mott}$	↗	0.147	1	1.666	3.290	3.308
$VC \left(10^{-4} \frac{V}{K}\right)$		0.503	↘ -4.87×10^{-6}	↘ -0.473	↘ -1.105	↘ -1.109
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.755	↗ 7.30×10^{-6}	↗ 0.710	↗ 1.657	↗ 1.664
Pt ($10^{-2}V$)		-0.314	↘ -0.9465	↘ -1.059	↘ -1.08915	↗ -1.0888

For $x=0.5$,

In the degenerate Ga- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(\Gamma_{Ga})$, one gets:

T(K)	↗	30	52.449	55	71.37119	71.5
ξ_p	↘	4.071	1.8138	1.674	1	0.996
$S \left(10^{-4} \frac{V}{K}\right)$		-1.162	-1.563	↗ -1.558	↗ -1.322	↗ -1.319
ZT		0.553	1	↘ 0.993	↘ 0.715	↘ 0.712

$(ZT)_{Mott}$	↗	0.198	1	1.174	3.290	3.318
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.576	2.37×10^{-5}	-0.143	-1.105	-1.112
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.863	-3.55×10^{-5}	0.215	1.657	1.668
Pt ($10^{-2}V$)	↘	-0.349	-0.820	-0.857	-0.9433	-0.9429

In the degenerate Mg- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{Mg})$, one gets:

T(K)	↗	30	60.028	70	81.68312	82
ξ_p	↘	4.681	1.8138	1.382	1	0.991
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.053	-1.563	-1.507	-1.322	-1.315
ZT	↗	0.454	1	0.930	0.715	0.708
$(ZT)_{Mott}$	↗	0.150	1	1.722	3.290	3.350
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.506	-2.49×10^{-5}	-0.505	-1.105	-1.120
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.760	3.73×10^{-5}	0.758	1.657	1.681
Pt ($10^{-2}V$)	↘	-0.316	-0.938	-1.0549	-1.07961	-1.07850

In the degenerate In- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{In})$, one gets:

T(K)	↗	30	60.442	70	82.246416	82.5
ξ_p	↘	4.712	1.8138	1.400	1	0.993
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.048	-1.563	-1.512	-1.322	-1.316
ZT	↗	0.449	1	0.936	0.715	0.709
$(ZT)_{Mott}$	↗	0.148	1	1.678	3.290	3.338
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.504	-2.67×10^{-5}	-0.480	-1.105	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.756	4.01×10^{-5}	0.720	1.657	1.676
Pt ($10^{-2}V$)	↘	-0.314	-0.945	-1.058	-1.08705	-1.0862

In the degenerate Cd- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{Cd})$, one gets:

T(K)	↗	30	60.8672	70	82.825577	83
ξ_p	↘	4.745	1.8138	1.419	1	0.995
$S \left(10^{-4} \frac{V}{K}\right)$	↘	-1.043	-1.563	-1.517	-1.322	-1.318
ZT	↗	0.450	1	0.942	0.715	0.711
$(ZT)_{Mott}$	↗	0.146	1	1.6634	3.290	3.323
$VC \left(10^{-4} \frac{V}{K}\right)$	↘	0.501	-6.78×10^{-6}	-0.455	-1.105	-1.114
$T_s \left(10^{-4} \frac{V}{K}\right)$	↗	-0.752	1.02×10^{-5}	0.682	1.657	1.670
Pt ($10^{-2}V$)	↘	-0.313	-0.951	-1.062	-1.09471	-1.09411

For x=1,

In the degenerate Ga- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{Ga})$, one gets:

T(K)	↗	30	52.177	55	71.00113	71.5
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ξ_p	↘	4.047	1.8138	1.659	1	0.983
$S \left(10^{-4} \frac{V}{K}\right)$		-1.166	↘ -1.563 ↗	-1.557	↗ -1.322 ↗	-1.310
ZT		0.557	↗ 1 ↘	0.992	↘ 0.715 ↘	0.702
$(ZT)_{Mott}$	↗	0.201	1	1.196	3.290	3.400
$VC \left(10^{-4} \frac{V}{K}\right)$		0.579	↘ 2.66×10^{-5} ↘	-0.160	↘ -1.105 ↘	-1.133
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.868	↗ -3.99×10^{-5} ↗	0.240	↗ 1.657 ↗	1.699
Pt ($10^{-2}V$)		-0.350	↘ -0.815 ↘	-0.856	↘ -0.938 ↗	-0.937

In the degenerate Mg- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{Mg})$, one gets:

T(K)	↗	30	59.716	70	81.259592	81.5
ξ_p	↘	4.657	1.8138	1.368	1	0.993
$S \left(10^{-4} \frac{V}{K}\right)$		-1.057	↘ -1.563 ↗	-1.503	↗ -1.322 ↗	-1.317
ZT		0.457	↗ 1 ↘	0.925	↘ 0.715 ↘	0.710
$(ZT)_{Mott}$	↗	0.152	1.0009	1.756	3.290	3.336
$VC \left(10^{-4} \frac{V}{K}\right)$		0.508	↘ 1.17×10^{-5} ↘	-0.524	↘ -1.105 ↘	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.763	↗ -1.76×10^{-5} ↗	0.786	↗ 1.657 ↗	1.675
Pt ($10^{-2}V$)		-0.317	↘ -0.933 ↘	-1.052	↘ -1.07401 ↗	-1.0732

In the degenerate In- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{In})$, one gets:

T(K)	↗	30	60.128	70	81.819968	82
ξ_p	↘	4.689	1.8138	1.386	1	0.995
$S \left(10^{-4} \frac{V}{K}\right)$		-1.052	↘ -1.563 ↗	-1.508	↗ -1.322 ↗	-1.318
ZT		0.453	↗ 1 ↘	0.931	↘ 0.715 ↘	0.711
$(ZT)_{Mott}$	↗	0.150	1	1.711	3.290	3.324
$VC \left(10^{-4} \frac{V}{K}\right)$		0.506	↘ 2.54×10^{-6} ↘	-0.499	↘ -1.105 ↘	-1.114
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.759	↗ -3.81×10^{-6} ↗	0.748	↗ 1.657 ↗	1.671
Pt ($10^{-2}V$)		-0.315	↘ -0.940 ↘	-1.056	↘ -1.081417 ↗	-1.0808

In the degenerate Cd- $InSb_{1-x}As_x$ alloy, for $N = 2 \times N_{CDP}(r_{Cd})$, one gets:

T(K)	↗	30	60.552	70	82.396125	82.5
ξ_p	↘	4.721	1.8138	1.405	1	0.997
$S \left(10^{-4} \frac{V}{K}\right)$		-1.046	↘ -1.563 ↗	-1.513	↗ -1.322 ↗	-1.320
ZT		0.448	↗ 1 ↘	0.937	↘ 0.715 ↘	0.713
$(ZT)_{Mott}$	↗	0.148	1	1.666	3.290	3.309
$VC \left(10^{-4} \frac{V}{K}\right)$		0.503	↘ -2.58×10^{-5} ↘	-0.473	↘ -1.105 ↘	-1.110
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.755	↗ 3.87×10^{-5} ↗	0.710	↗ 1.657 ↗	1.665
Pt ($10^{-2}V$)		-0.314	↘ -0.946 ↘	-1.059	↘ -1.08903 ↗	-1.0887

Table 6n. Here, for a given T and with decreasing N, the reduced Fermi-energy ξ_n decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T: (i) for $\xi_n \approx 1.8138$, while the numerical results of S present a same minimum $(S)_{\min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$, those of ZT show a same maximum $(ZT)_{\max} = 1$, (ii) for $\xi_n = 1$, those of S, ZT, $(ZT)_{\text{Mott}}$, VC, and T_s present the same results: $-1.322 \times 10^{-4} \frac{V}{K}$, 0.715, 3.290, $-1.105 \times 10^{-4} \frac{V}{K}$, and $1.657 \times 10^{-4} \frac{V}{K}$, respectively, and (iii) for $\xi_n \approx 1.8138$, $(ZT)_{\text{Mott}} = 1$.

For x=0,

In the degenerate P- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T= 10.528 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	3	2.5942062	2.3	2.11428385	2.11
ξ_n	↘	2.42542	1.8138	1.336	1	0.992
$S(10^{-4} \frac{V}{K})$		-1.499	↘ -1.563 ↗	-1.493	↗ -1.322 ↗	-1.316
ZT		0.920	↗ 1 ↘	0.912	↘ 0.715 ↘	0.709
$(ZT)_{\text{Mott}}$	↗	0.559	1	1.844	3.290	3.345
$VC(10^{-4} \frac{V}{K})$		0.438	↘ -7.52×10^{-5} ↘	-0.571	↘ -1.105 ↘	-1.119
$T_s(10^{-4} \frac{V}{K})$		-0.657	↗ 1.13×10^{-4} ↗	0.856	↗ 1.657 ↗	1.678
Pt ($10^{-3}V$)		-1.578	↘ -1.645 ↗	-1.571	↗ -1.391 ↗	-1.385

In the degenerate As- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T= 12.813 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4	3.4831608	3	2.8387545	2.838
ξ_n	↘	2.395	1.8138	1.221	1	0.999
$S(10^{-4} \frac{V}{K})$		-1.504	↘ -1.563 ↗	-1.448	↗ -1.322 ↗	-1.3209
ZT		0.927	↗ 1 ↘	0.858	↘ 0.715 ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.574	1	2.206	3.290	3.297
$VC(10^{-4} \frac{V}{K})$		0.422	↘ -2.35×10^{-5} ↘	-0.742	↘ -1.105 ↘	-1.107
$T_s(10^{-4} \frac{V}{K})$		-0.633	↗ 3.53×10^{-5} ↗	1.114	↗ 1.657 ↗	1.660
Pt ($10^{-3}V$)		-1.928	↘ -2.003 ↗	-1.856	↗ -1.693 ↗	-1.692

In the degenerate Sb- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T= 15.0335 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4.5	4.4268778	4	3.6078456	3.607
ξ_n	↘	1.880	1.8138	1.411	1	0.999
$S(10^{-4} \frac{V}{K})$		-1.562	↘ -1.563 ↗	-1.514	↗ -1.322 ↗	-1.321
ZT		0.999	↗ 1 ↘	0.939	↘ 0.715 ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.930	1	1.653	3.290	3.296
$VC(10^{-4} \frac{V}{K})$		0.422	↘ 2.14×10^{-5} ↘	-0.466	↘ -1.105 ↘	-1.106
$T_s(10^{-4} \frac{V}{K})$		-0.092	↗ -3.22×10^{-5} ↗	0.699	↗ 1.657 ↗	1.660
Pt ($10^{-3}V$)		-2.348	↘ -2.350 ↗	-2.277	↗ -1.987 ↗	-1.986

In the degenerate Sn- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T=15.1525 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	5	4.4794468	4	3.6507193	3.65
ξ_n	↘	2.271	1.8138	1.364	1	0.999
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.524 ↘	-1.563 ↗	-1.502 ↗	-1.322 ↗	-1.321
ZT	↗ ↘	0.951 ↗	1 ↘	0.923 ↘	0.715 ↘	0.714
$(ZT)_{\text{Mott}}$	↗ ↘	0.638 ↗	1 ↘	1.768 ↘	3.290 ↘	3.295
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.353 ↘	-2.06×10^{-5} ↘	-0.530 ↘	-1.105 ↘	-1.106
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.529 ↗	3.08×10^{-5} ↗	0.796 ↗	1.657 ↗	1.659
$Pt(10^{-3}V)$	↘ ↗	-2.310 ↘	-2.368 ↗	-2.275 ↗	-2.003 ↗	-2.002

For x=0.5,

In the degenerate P- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T=11.4883 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	3	2.7382966	2.5	2.2316667	2.23
ξ_n	↘	2.191	1.8138	1.452	1	0.997
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.535 ↘	-1.563 ↗	-1.525 ↗	-1.322 ↗	-1.319
ZT	↗ ↘	0.965 ↗	1 ↘	0.952 ↘	0.715 ↘	0.713
$(ZT)_{\text{Mott}}$	↗ ↘	0.685 ↗	1 ↘	1.561 ↘	3.290 ↘	3.310
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.303 ↘	3.95×10^{-5} ↘	-0.411 ↘	-1.105 ↘	-1.110
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.454 ↗	-5.92×10^{-5} ↗	0.616 ↗	1.657 ↗	1.665
$Pt(10^{-3}V)$	↘ ↗	-1.764 ↘	-1.796 ↗	-1.752 ↗	-1.518 ↗	-1.516

In the degenerate As- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T=13.9822 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	4	3.6766266	3.5	2.99641842	2.99
ξ_n	↘	2.162	1.8138	1.617	1	0.991
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.539 ↘	-1.563 ↗	-1.553 ↗	-1.322 ↗	-1.315
ZT	↗ ↘	0.970 ↗	1 ↘	0.987 ↘	0.715 ↘	0.708
$(ZT)_{\text{Mott}}$	↗ ↘	0.704 ↗	1 ↘	1.258 ↘	3.290 ↘	3.348
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.283 ↘	-7.62×10^{-6} ↘	-0.207 ↘	-1.105 ↘	-1.120
$T_s(10^{-4}\frac{V}{K})$	↗ ↘	-0.424 ↗	1.14×10^{-5} ↗	0.310 ↗	1.657 ↗	1.680
$Pt(10^{-3}V)$	↘ ↗	-2.152 ↘	-2.185 ↗	-2.171 ↗	-1.848 ↗	-1.839

In the degenerate Sb- $\text{InSb}_{1-x}\text{As}_x$ alloy, for T=16.4055 K, one gets:

$N(10^{16}\text{cm}^{-3})$	↘	5	4.6727606	4	3.8082485	3.80
ξ_n	↘	2.092	1.8138	1.197	1	0.991
$S(10^{-4}\frac{V}{K})$	↘ ↗	-1.547 ↘	-1.563 ↗	-1.437 ↗	-1.322 ↗	-1.315
ZT	↗ ↘	0.980 ↗	1 ↘	0.845 ↘	0.715 ↘	0.708
$(ZT)_{\text{Mott}}$	↗ ↘	0.752 ↗	1 ↘	2.296 ↘	3.290 ↘	3.348
$VC(10^{-4}\frac{V}{K})$	↘ ↗	0.234 ↘	6.02×10^{-6} ↘	-0.780 ↘	-1.105 ↘	-1.120

$T_s (10^{-4} \frac{V}{K})$	-0.350	$\nearrow -9.03 \times 10^{-6}$	$\nearrow 1.171$	$\nearrow 1.657$	$\nearrow 1.680$
$Pt (10^{-3}V)$	-2.538	$\searrow -2.564$	$\nearrow -2.357$	$\nearrow -2.168$	$\nearrow -2.158$

In the degenerate Sn- $InSb_{1-x}As_x$ alloy, for T=16.535 K one gets:

$N(10^{16}cm^{-3})$	$\searrow 5$	4.7282496	4	3.8534551	3.85
ξ_n	$\searrow 2.042$	1.8138	1.150	1	0.996
$S (10^{-4} \frac{V}{K})$	-1.552	$\searrow -1.563$	$\nearrow -1.414$	$\nearrow -1.322$	$\nearrow -1.319$
ZT	0.986	$\nearrow 1$	$\searrow 0.818$	$\searrow 0.715$	$\searrow 0.712$
$(ZT)_{Mott}$	$\nearrow 0.788$	1	2.488	3.290	3.314
$VC (10^{-4} \frac{V}{K})$	0.197	$\searrow 2.73 \times 10^{-5}$	$\searrow -0.855$	$\searrow -1.105$	$\searrow -1.111$
$T_s (10^{-4} \frac{V}{K})$	-0.295	$\nearrow -4.09 \times 10^{-5}$	$\nearrow 1.283$	$\nearrow 1.657$	$\nearrow 1.667$
$Pt (10^{-3}V)$	-2.566	$\searrow -2.584$	$\nearrow -2.337$	$\nearrow -2.185$	$\nearrow -2.181$

For x=1,

In the degenerate P- $InSb_{1-x}As_x$ alloy, for T=12.633 K, one gets:

$N(10^{16}cm^{-3})$	$\searrow 3$	2.9111922	2.5	2.37260017	2.37
ξ_n	$\searrow 1.936$	1.8138	1.209	1	0.995
$S (10^{-4} \frac{V}{K})$	-1.560	$\searrow -1.563$	$\nearrow -1.443$	$\nearrow -1.322$	$\nearrow -1.318$
ZT	0.996	$\nearrow 1$	$\searrow 0.852$	$\searrow 0.715$	$\searrow 0.712$
$(ZT)_{Mott}$	$\nearrow 0.878$	1	2.249	3.290	3.319
$VC (10^{-4} \frac{V}{K})$	0.110	$\searrow -2.46 \times 10^{-4}$	$\searrow -0.761$	$\searrow -1.105$	$\searrow -1.113$
$T_s (10^{-4} \frac{V}{K})$	-0.165	$\nearrow 3.69 \times 10^{-4}$	$\nearrow 1.141$	$\nearrow 1.657$	$\nearrow 1.669$
$Pt (10^{-3}V)$	-1.970	$\searrow -1.974$	$\nearrow -1.823$	$\nearrow -1.669$	$\nearrow -1.665$

In the degenerate As- $InSb_{1-x}As_x$ alloy, for T=15.3737 K, one gets:

$N(10^{16}cm^{-3})$	$\searrow 4$	3.9087682	3.5	3.18559	3.18
ξ_n	$\searrow 1.907$	1.8138	1.375	1	0.993
$S (10^{-4} \frac{V}{K})$	-1.561	$\searrow -1.563$	$\nearrow -1.505$	$\nearrow -1.322$	$\nearrow -1.317$
ZT	0.997	$\nearrow 1$	$\searrow 0.927$	$\searrow 0.715$	$\searrow 0.710$
$(ZT)_{Mott}$	$\nearrow 0.904$	1	1.740	3.290	3.337
$VC (10^{-4} \frac{V}{K})$	0.086	$\searrow 2.66 \times 10^{-5}$	$\searrow -0.515$	$\searrow -1.105$	$\searrow -1.117$
$T_s (10^{-4} \frac{V}{K})$	-0.129	$\nearrow -4.00 \times 10^{-5}$	$\nearrow 0.773$	$\nearrow 1.657$	$\nearrow 1.676$
$Pt (10^{-3}V)$	-2.400	$\searrow -2.403$	$\nearrow -2.313$	$\nearrow -2.032$	$\nearrow -2.024$

In the degenerate Sb- $InSb_{1-x}As_x$ alloy, for T=18.0385 K, one gets:

$N(10^{16}cm^{-3})$	$\searrow 5.5$	4.9677978	4.5	4.0487165	4.045
ξ_n	$\searrow 2.236$	1.8138	1.420	1	0.996
$S (10^{-4} \frac{V}{K})$	-1.529	$\searrow -1.563$	$\nearrow -1.517$	$\nearrow -1.322$	$\nearrow -1.319$

ZT	0.957 ↗	1 ↘	0.942 ↘	0.715 ↘	0.712
$(ZT)_{Mott}$ ↗	0.658	1	1.630	3.290	3.314
$VC \left(10^{-4} \frac{V}{K}\right)$	0.331 ↘	-1.36×10^{-5} ↘	-0.452 ↘	-1.105 ↘	-1.111
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.497 ↗	2.04×10^{-5} ↗	0.679 ↗	1.657 ↗	1.667
$Pt (10^{-3}V)$	-2.759 ↘	-2.819 ↗	-2.737 ↗	-2.384 ↗	-2.379

In the degenerate Sn- $InSb_{1-x}As_x$ alloy, for T=18.1809 K, one gets:

$N(10^{16}cm^{-3})$	↘ 5.5	5.0267904	4.5	4.0967788	4.096
ξ_n	↘ 2.186	1.8138	1.374	1	0.999
$S \left(10^{-4} \frac{V}{K}\right)$	-1.536 ↘	-1.563 ↗	-1.505 ↗	-1.322 ↗	-1.321
ZT	0.966 ↗	1 ↘	0.927 ↘	0.715 ↘	0.714
$(ZT)_{Mott}$ ↗	0.689	1	1.742	3.290	3.295
$VC \left(10^{-4} \frac{V}{K}\right)$	0.299 ↘	6.15×10^{-6} ↘	-0.516 ↘	-1.105 ↘	-1.106
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.448 ↗	-9.23×10^{-6} ↗	0.775 ↗	1.657 ↗	1.659
$Pt (10^{-3}V)$	-2.793 ↘	-2.842 ↗	-2.735 ↗	-2.403 ↗	-2.402

Table 6p. Here, for a given T and with decreasing N, the reduced Fermi-energy ξ_p decreases, and other thermoelectric coefficients are in variations, as indicated by the arrows as: (increase: ↗, decrease: ↘). One notes here that with increasing T: (i) for $\xi_p \approx 1.8138$, while the numerical results of S present a same minimum $(S)_{min.} (\approx -1.563 \times 10^{-4} \frac{V}{K})$, those of ZT show a same maximum $(ZT)_{max.} = 1$, (ii) for $\xi_p = 1$, those of S, ZT, $(ZT)_{Mott}$, VC, and T_s present the same results: $-1.322 \times 10^{-4} \frac{V}{K}$, 0.715, 3.290, $-1.105 \times 10^{-4} \frac{V}{K}$, and $1.657 \times 10^{-4} \frac{V}{K}$, respectively, and (iii) for $\xi_p \approx 1.8138$, $(ZT)_{Mott} = 1$.

For x=0,

In the degenerate Ga- $InSb_{1-x}As_x$ alloy, for T=52.183 K, one gets:

$N(10^{18}cm^{-3})$	↘ 2.5	2.2902686	2	1.8665455	1.866
ξ_p	↘ 2.176	1.8138	1.276	1	0.999
$S \left(10^{-4} \frac{V}{K}\right)$	-1.537 ↘	-1.563 ↗	-1.471 ↗	-1.322 ↗	-1.321
ZT	0.968 ↗	1 ↘	0.886 ↘	0.715 ↘	0.714
$(ZT)_{Mott}$ ↗	0.695	1	2.021	3.290	3.298
$VC \left(10^{-4} \frac{V}{K}\right)$	0.292 ↘	1.35×10^{-6} ↘	-0.659 ↘	-1.105 ↘	-1.107
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.438 ↗	-2.03×10^{-6} ↗	0.988 ↗	1.657 ↗	1.660
$Pt (10^{-3}V)$	-8.023 ↘	-8.156 ↗	-7.676 ↗	-6.897 ↗	-6.893

In the degenerate Mg- $InSb_{1-x}As_x$ alloy, for T=59.722 K, one gets:

$N(10^{18}cm^{-3})$	↘ 3	2.8041452	2.5	2.2853372	2.28
ξ_p	↘ 2.091	1.8138	1.358	1	0.990

$S \left(10^{-4} \frac{V}{K}\right)$	-1.547	↘	-1.563	↗	-1.500	↗	-1.322	↗	-1.315
ZT	0.980	↗	1	↘	0.921	↘	0.715	↘	0.708
$(ZT)_{Mott}$	↗ 0.752		1		1.784		3.290		3.353
$VC \left(10^{-4} \frac{V}{K}\right)$	0.233	↘	2.86×10^{-5}	↘	-0.539	↘	-1.105	↘	-1.121
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.350	↗	-4.30×10^{-5}	↗	0.809	↗	1.657	↗	1.682
Pt ($10^{-3}V$)	-9.241	↘	-9.334	↗	-8.956	↗	-7.893	↗	-7.853

In the degenerate In- $InSb_{1-x}As_x$ alloy, for T=60.135 K, one gets:

$N(10^{18}cm^{-3})$	↘ 3		2.8332018		2.5		2.30904345		2.305
ξ_p	↘ 2.048		1.8138		1.317		1		0.993
$S \left(10^{-4} \frac{V}{K}\right)$	-1.551	↘	-1.563	↗	-1.486	↗	-1.322	↗	-1.317
ZT	0.985	↗	1	↘	0.904	↘	0.715	↘	0.710
$(ZT)_{Mott}$	↗ 0.784		1		1.896		3.290		3.337
$VC \left(10^{-4} \frac{V}{K}\right)$	0.201	↘	-2.68×10^{-5}	↘	-0.598	↘	-1.105	↘	-1.117
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.301	↗	4.02×10^{-5}	↗	0.897	↗	1.657	↗	1.676
Pt ($10^{-3}V$)	-9.330	↘	-9.399	↗	-8.937	↗	-7.948	↗	-7.918

In the degenerate Cd- $InSb_{1-x}As_x$ alloy, for T=60.558 K, one gets:

$N(10^{18}cm^{-3})$	↘ 3		2.8631806		2.5		2.3334658		2.333
ξ_p	↘ 2.004		1.8138		1.275		1		0.994
$S \left(10^{-4} \frac{V}{K}\right)$	-1.555	↘	-1.563	↗	-1.471	↗	-1.322	↗	-1.317
ZT	0.990	↗	1	↘	0.885	↘	0.715	↘	0.710
$(ZT)_{Mott}$	↗ 0.819		1		2.022		3.290		3.330
$VC \left(10^{-4} \frac{V}{K}\right)$	0.167	↘	-4.87×10^{-6}	↘	-0.659	↘	-1.105	↘	-1.115
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.250	↗	7.30×10^{-6}	↗	0.989	↗	1.657	↗	1.673
Pt ($10^{-3}V$)	-9.418	↘	-9.465	↗	-8.907	↗	-8.004	↗	-7.978

For x=0.5,

In the degenerate Ga- $InSb_{1-x}As_x$ alloy, for T=52.449 K, one gets:

$N(10^{18}cm^{-3})$	↘ 2		1.8889296		1.7		1.53945142		1.539
ξ_p	↘ 2.048		1.8138		1.395		1		0.999
$S \left(10^{-4} \frac{V}{K}\right)$	-1.551	↘	-1.563	↗	-1.511	↗	-1.322	↗	-1.321
ZT	0.985	↗	1	↘	0.934	↘	0.715	↘	0.714
$(ZT)_{Mott}$	↗ 0.784		1		1.690		3.290		3.298
$VC \left(10^{-4} \frac{V}{K}\right)$	0.201	↘	2.37×10^{-5}	↘	-0.487	↘	-1.105	↘	-1.107
$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.301	↗	-3.55×10^{-5}	↗	0.731	↗	1.657	↗	1.660
Pt ($10^{-2}V$)	-0.814	↘	-0.820	↗	-0.792	↗	-0.6932	↗	-0.6928

In the degenerate Mg- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $T=60.028$ K, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	2.3127562	2.2	1.88488252	1.88
ξ_p	↘	2.134	1.8138	1.614	1	0.989
$S(10^{-4}\frac{V}{K})$		-1.542	↘ -1.563 ↗	-1.552	↗ -1.322 ↗	-1.314
ZT		0.974	↗ 1 ↘	0.986	↘ 0.715 ↘	0.707
$(ZT)_{\text{Mott}}$	↗	0.722	1	1.263	3.290	3.360
$VC(10^{-4}\frac{V}{K})$		0.264	↘ -2.497×10^{-5} ↘	-0.210	↘ -1.105 ↘	-1.123
$T_s(10^{-4}\frac{V}{K})$		-0.396	↗ 3.73×10^{-5} ↗	0.316	↗ 1.657 ↗	1.684
Pt ($10^{-2}V$)		-0.926	↘ -0.938 ↗	-0.932	↗ -0.79339 ↗	-0.7889

In the degenerate In- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $T=60.442K$, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	2.336721	2.2	1.9044144	1.904
ξ_p	↘	2.091	1.8138	1.573	1	0.999
$S(10^{-4}\frac{V}{K})$		-1.547	↘ -1.563 ↗	-1.547	↗ -1.322 ↗	-1.321
ZT		0.980	↗ 1 ↘	0.980	↘ 0.715 ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.752	1	1.329	3.290	3.296
$VC(10^{-4}\frac{V}{K})$		0.233	↘ -2.67×10^{-5} ↘	-0.258	↘ -1.105 ↘	-1.106
$T_s(10^{-4}\frac{V}{K})$		-0.350	↗ 4.01×10^{-5} ↗	0.387	↗ 1.657 ↗	1.660
Pt ($10^{-2}V$)		-0.935	↘ -0.945 ↗	-0.935	↗ -0.7989 ↗	-0.7985

In the degenerate Cd- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $T=60.8672K$, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2.5	2.3614464	2.2	1.9245578	1.924
ξ_p	↘	2.047	1.8138	1.531	1	0.999
$S(10^{-4}\frac{V}{K})$		-1.552	↘ -1.563 ↗	-1.541	↗ -1.322 ↗	-1.321
ZT		0.985	↗ 1 ↘	0.972	↘ 0.715 ↘	0.714
$(ZT)_{\text{Mott}}$	↗	0.785	1	1.403	3.290	3.298
$VC(10^{-4}\frac{V}{K})$		0.200	↘ -6.78×10^{-6} ↘	-0.309	↘ -1.105 ↘	-1.107
$T_s(10^{-4}\frac{V}{K})$		-0.300	↗ 1.02×10^{-5} ↗	0.463	↗ 1.657 ↗	1.660
Pt ($10^{-2}V$)		-0.944	↘ -0.951 ↗	-0.938	↗ -0.80448 ↗	-0.80398

For $x=1$,

In the degenerate Ga- $\text{InSb}_{1-x}\text{As}_x$ alloy, for $T=52.177$ K, one gets:

$N(10^{18}\text{cm}^{-3})$	↘	2	1.4873359	1.45	1.21215745	1.21
ξ_p	↘	3.120	1.8138	1.712	1	0.993
$S(10^{-4}\frac{V}{K})$		-1.358	↘ -1.563 ↗	-1.560	↗ -1.322 ↗	-1.316
ZT		0.755	↗ 1 ↘	0.997	↘ 0.715 ↘	0.709
$(ZT)_{\text{Mott}}$	↗	0.338	1	1.123	3.290	3.338
$VC(10^{-4}\frac{V}{K})$		0.639	↘ 2.66×10^{-5} ↘	-0.103	↘ -1.105 ↘	-1.117

$T_s \left(10^{-4} \frac{V}{K}\right)$	-0.958	$\nearrow -3.99 \times 10^{-5}$	\nearrow	0.154	\nearrow	1.657	\nearrow	1.676	
Pt ($10^{-2}V$)	-0.709	\searrow	-0.815	\nearrow	-0.814	\nearrow	-0.6896	\nearrow	-0.6869

In the degenerate Mg- $InSb_{1-x}As_x$ alloy, for T=59.716 K, one gets:

$N(10^{18}cm^{-3})$	\searrow	2.5	1.8210554	1.6	1.4841384	1.484				
ξ_p	\searrow	3.218	1.8138	1.300	1	0.999				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.337	\searrow	-1.563	\nearrow	-1.480	\nearrow	-1.322	\nearrow	-1.321
ZT		0.732	\nearrow	1	\searrow	0.897	\searrow	0.715	\searrow	0.7148
$(ZT)_{Mott}$	\nearrow	0.318		1.0009		1.946		3.290		3.292
$VC \left(10^{-4} \frac{V}{K}\right)$		0.645	\searrow	1.17×10^{-5}	\searrow	-0.623	\searrow	-1.105	\searrow	-1.1056
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.968	\nearrow	-1.76×10^{-5}	\nearrow	0.934	\nearrow	1.657	\nearrow	1.658
Pt ($10^{-2}V$)		-0.798	\searrow	-0.933	\nearrow	-0.884	\nearrow	-0.7893	\nearrow	-0.7891

In the degenerate In- $InSb_{1-x}As_x$ alloy, for T=60.128 K, one gets:

$N(10^{18}cm^{-3})$	\searrow	2.5	1.8399251	1.6	1.499519795	1.498				
ξ_p	\searrow	3.169	1.8138	1.259	1	0.996				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.348	\searrow	-1.563	\nearrow	-1.464	\nearrow	-1.322	\nearrow	-1.319
ZT		0.743	\nearrow	1	\searrow	0.878	\searrow	0.715	\searrow	0.712
$(ZT)_{Mott}$	\nearrow	0.327		1		2.074		3.290		3.317
$VC \left(10^{-4} \frac{V}{K}\right)$		0.643	\searrow	2.54×10^{-6}	\searrow	-0.684	\searrow	-1.105	\searrow	-1.112
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.964	\nearrow	-3.81×10^{-6}	\nearrow	1.026	\nearrow	1.657	\nearrow	1.668
Pt ($10^{-2}V$)		-0.810	\searrow	-0.940	\nearrow	-0.880	\nearrow	-0.795	\nearrow	-0.793

In the degenerate Cd- $InSb_{1-x}As_x$ alloy, for T=60.552 K, one gets:

$N(10^{18}cm^{-3})$	\searrow	2.5	1.8593938	1.6	1.51539518	1.515				
ξ_p	\searrow	3.119	1.8138	1.217	1	0.999				
$S \left(10^{-4} \frac{V}{K}\right)$		-1.358	\searrow	-1.563	\nearrow	-1.445	\nearrow	-1.322	\nearrow	-1.321
ZT		0.755	\nearrow	1	\searrow	0.856	\searrow	0.715	\searrow	0.714
$(ZT)_{Mott}$	\nearrow	0.338		1		2.219		3.290		3.297
$VC \left(10^{-4} \frac{V}{K}\right)$		0.639	\searrow	-2.58×10^{-5}	\searrow	-0.748	\searrow	-1.105	\searrow	-1.107
$T_s \left(10^{-4} \frac{V}{K}\right)$		-0.958	\nearrow	3.87×10^{-5}	\nearrow	0.112	\nearrow	1.657	\nearrow	1.660
Pt ($10^{-2}V$)		-0.822	\searrow	-0.946	\nearrow	-0.876	\nearrow	-0.800	\nearrow	-0.7998